

Special Purpose Reservoir Simulators

1-Basic Equations and Concepts

Basic Differential Equations for Flow in Reservoir Engineering

(Note: A similar approach is possible with energy and entropy equations)

Material Balance for One Component in One Phase

$$\frac{\partial}{\partial t}(\varepsilon_j \rho_j \omega_{ij}) + \vec{\nabla} \cdot \left[\rho_j \omega_{ij} \vec{u}_j - \varepsilon_j \vec{K}_{ij} \cdot \vec{\nabla} \rho_j \omega_{ij} \right] = \varepsilon_j r_{ij} + r_{mij} \quad i=1, \dots, N_C \quad j=1, \dots, N_P$$

$$\sum_{i=1}^{N_P} ()$$

$$\sum_{i=1}^{N_C} ()$$

Overall Compositional Equations

$$\frac{\partial}{\partial t} \left(\phi \sum_{j=1}^{N_P} S_j \rho_j \omega_{ij} + (1-\phi) \rho_s \omega_{is} \right) + \vec{\nabla} \cdot \left[\sum_{j=1}^{N_P} \left(\rho_j \omega_{ij} \vec{u}_j - \phi S_j \vec{K}_{ij} \cdot \vec{\nabla} (\rho_j \omega_{ij}) \right) \right] = \phi \sum_{j=1}^{N_P} S_j r_{ij} + (1-\phi) r_{is}, \quad i=1, \dots, N_C$$

Phase Flow Equations

$$\frac{\partial}{\partial t} (\phi S_j \rho_j) + \vec{\nabla} \cdot (\rho_j \vec{u}_j) = \sum_{i=1}^{N_C} r_{mij}, \quad j=1, \dots, N_P$$

$$\sum_{i=1}^{N_C} ()$$

$$\sum_{i=1}^{N_P} ()$$

Continuity Equation

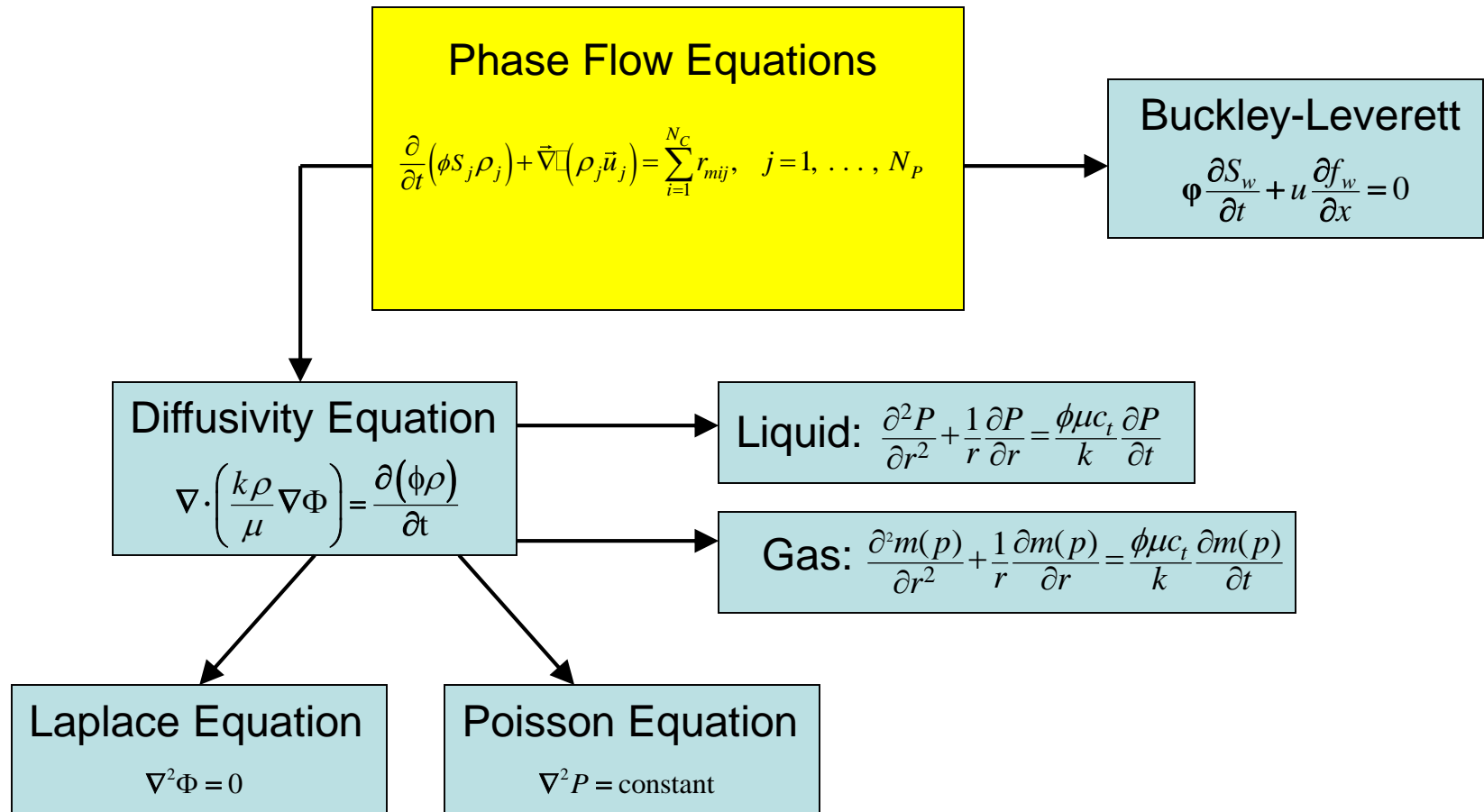
$$\frac{\partial}{\partial t} \left(\phi \sum_{j=1}^{N_P} \rho_j S_j + (1-\phi) \rho_s \right) + \vec{\nabla} \cdot \left[\sum_{j=1}^{N_P} \rho_j \vec{u}_j \right] = 0$$

Note:

$$\varepsilon_j = \phi S_j \quad \text{for fluids}$$

$$\varepsilon_s = 1 - \phi \quad \text{for solids}$$

Special Cases of Phase Flow Equations



Special Cases of Overall Compositional Equations

Overall Compositional Equations

$$\frac{\partial}{\partial t} \left(\phi \sum_{j=1}^{N_P} S_j \rho_j \omega_{ij} + (1-\phi) \rho_s \omega_{is} \right) + \vec{\nabla} \cdot \left[\sum_{j=1}^{N_P} \left(\rho_j \omega_{ij} \vec{u}_j - \phi S_j \vec{K}_{ij} \cdot \vec{\nabla} (\rho_j \omega_{ij}) \right) \right]$$

$$= \phi \sum_{j=1}^{N_P} S_j r_{ij} + (1-\phi) r_{is}, \quad i=1, \dots, N_C$$

Convection-Dispersion Equations

$$\phi \frac{\partial C_i}{\partial t} + u \frac{\partial C_i}{\partial x} = \phi K_{li} \frac{\partial^2 C_i}{\partial x^2}, \quad i=1, \dots, N_C$$

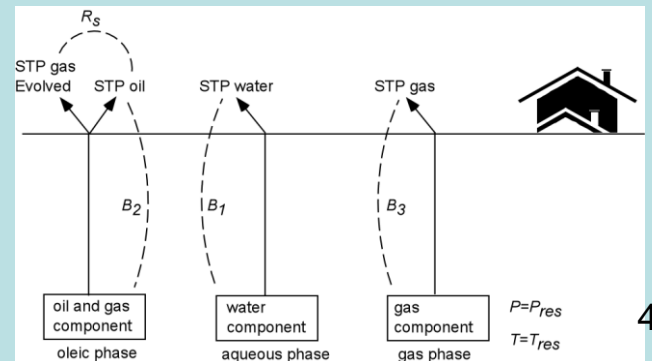
Dispersion-Free Overall Compositional Equations

$$\phi \frac{\partial C_i}{\partial t} + u \frac{\partial F_i}{\partial x} = 0, \quad i=1, \dots, N_C$$

Black-Oil Equations

$$\frac{\partial}{\partial t} \left(\frac{\phi S_j}{B_j} \right) + \vec{\nabla} \cdot \left(\frac{\vec{u}_j}{B_j} \right) = 0, \quad j = o, w$$

$$\frac{\partial}{\partial t} \left(\phi \left[\frac{S_g}{B_g} + \frac{S_o R_s}{B_o} \right] \right) + \vec{\nabla} \cdot \left(\frac{R_s}{B_o} \vec{u}_o + \frac{\vec{u}_g}{B_g} \right) = 0$$



Basic Oil Recovery Equation

$$N_p = \frac{E_V E_D S_{OI} V_P}{B_O}$$

E_V = Volumetric sweep efficiency = $E_A E_I$

N_p = Cumulative oil recovery

E_A = Areal sweep efficiency

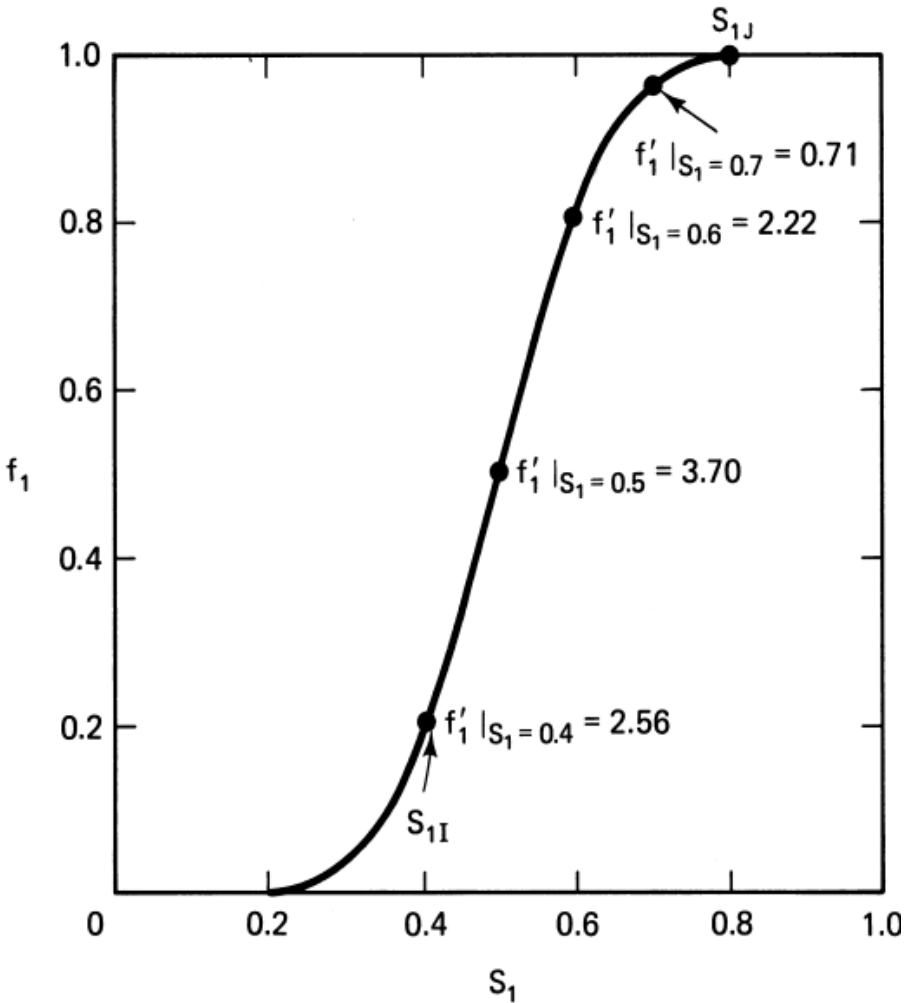
E_I = Vertical sweep efficiency

E_D = Displacement (local) sweep efficiency

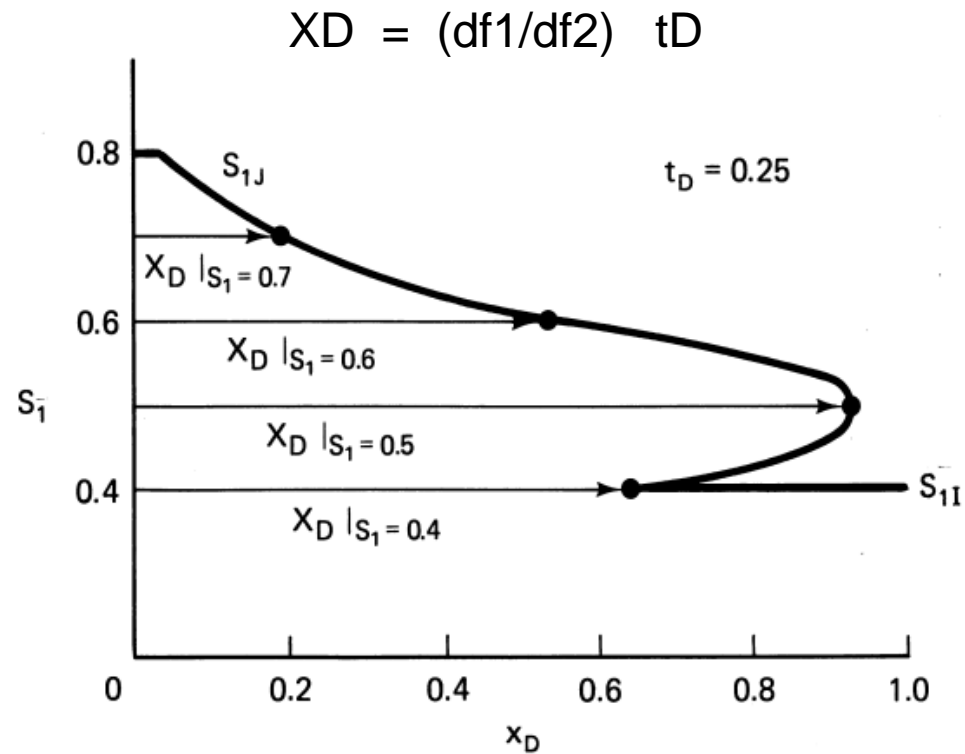
S_{OI} = Initial oil saturation

V_P = Pore volume

Buckley-Leverett construction of $S_1(x_D, t_D)$

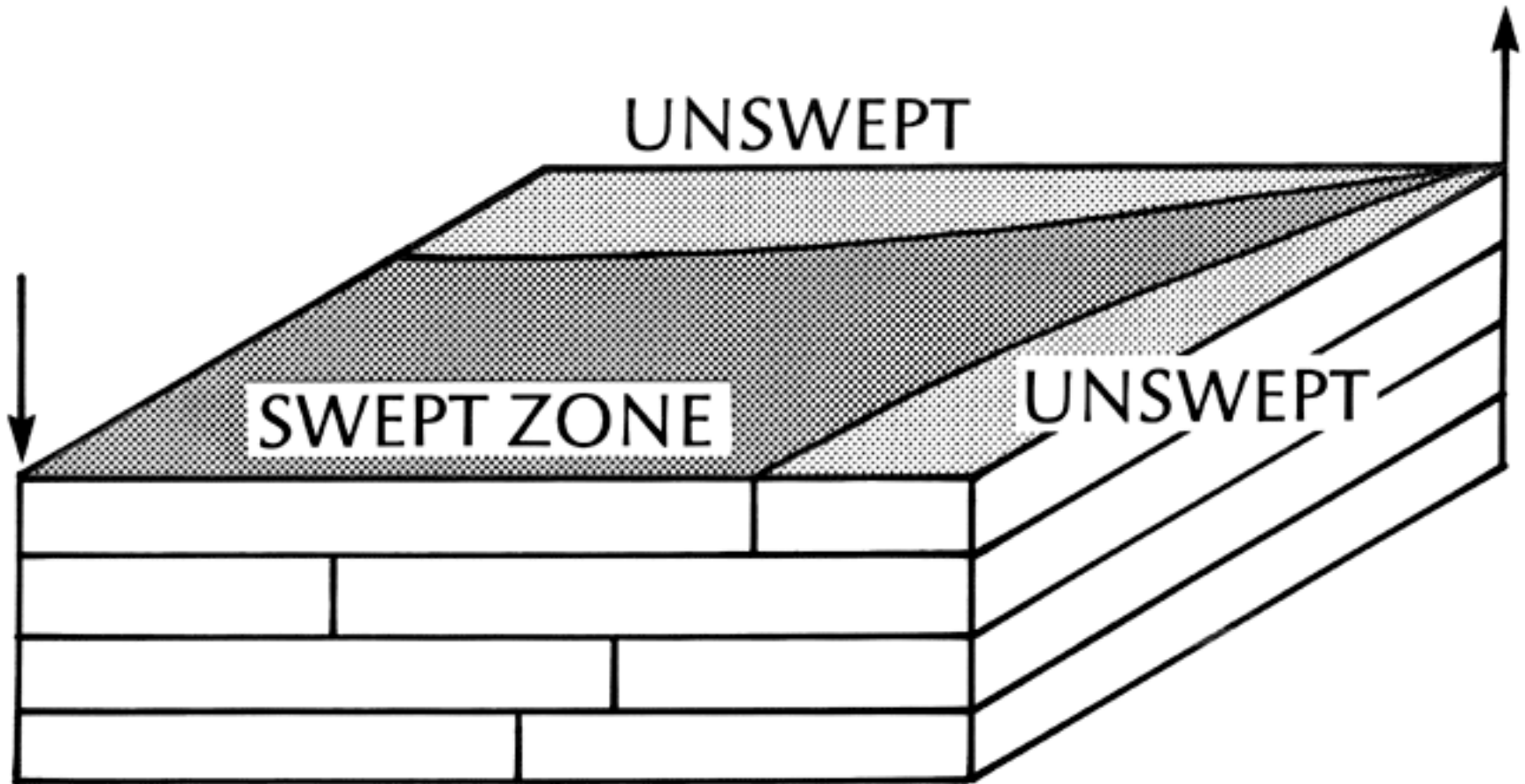


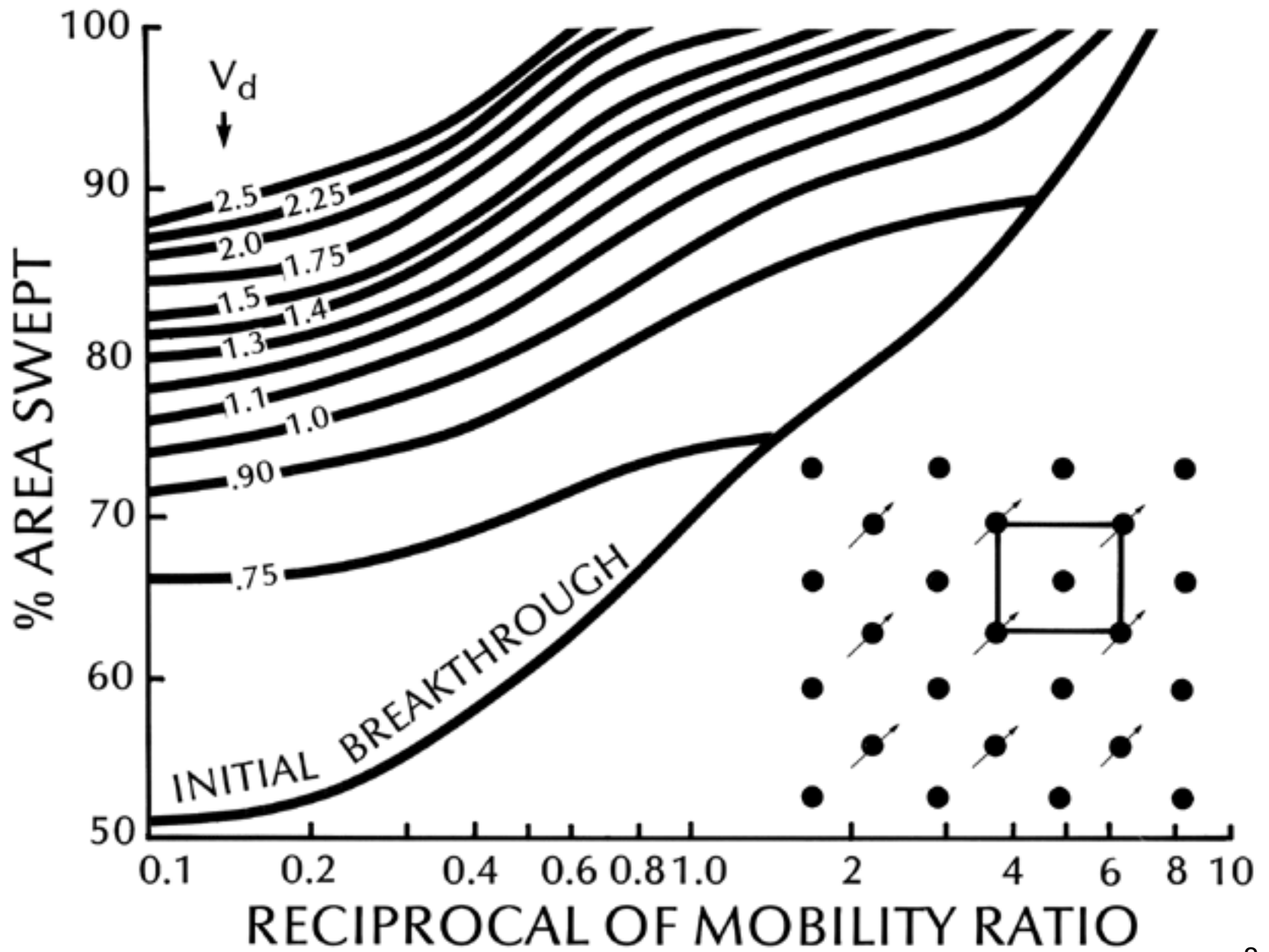
(a) Slopes of a fractional flow curve



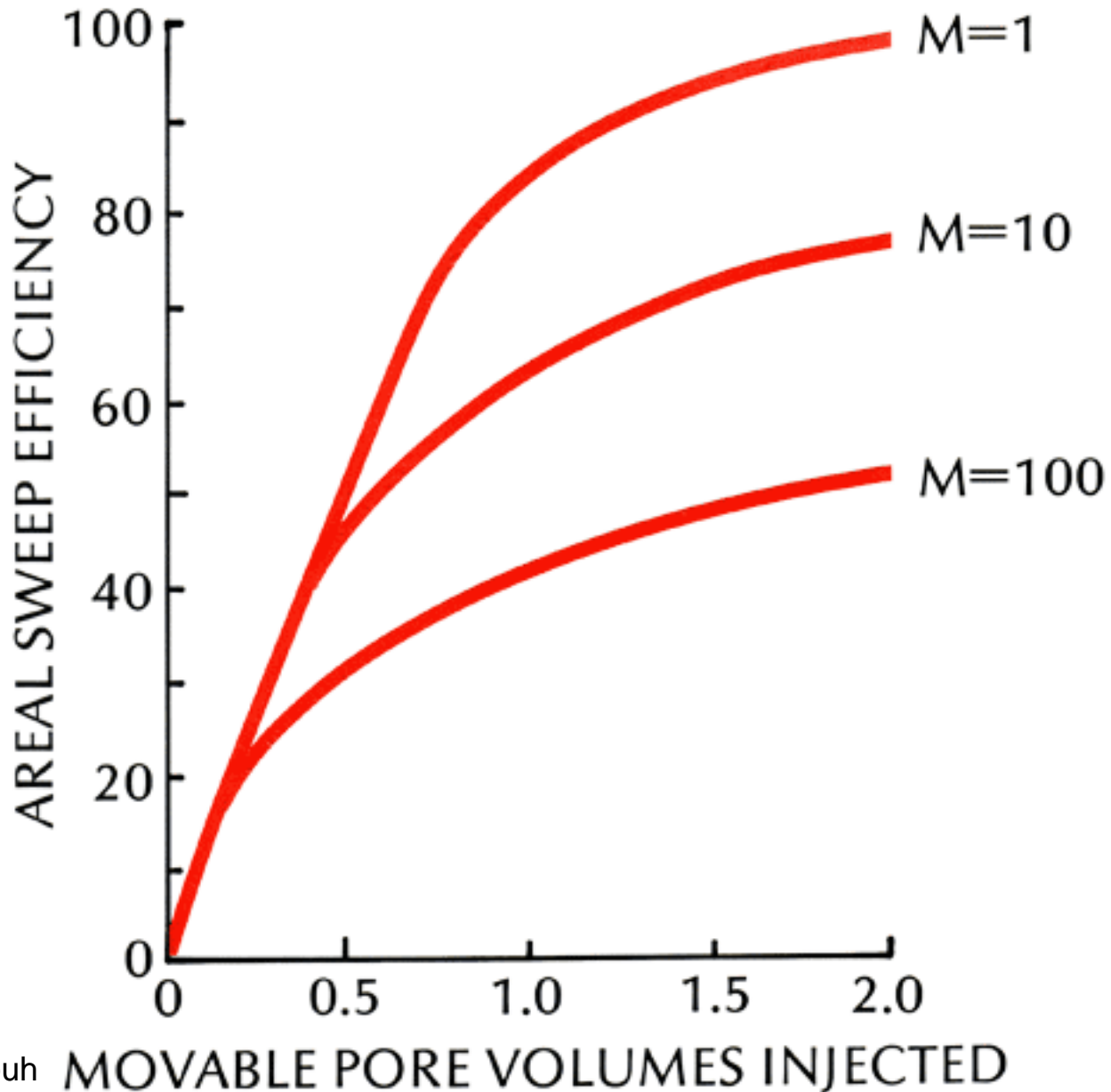
(b) Corresponding saturation profile

Areal Sweep Efficiency Schematic...

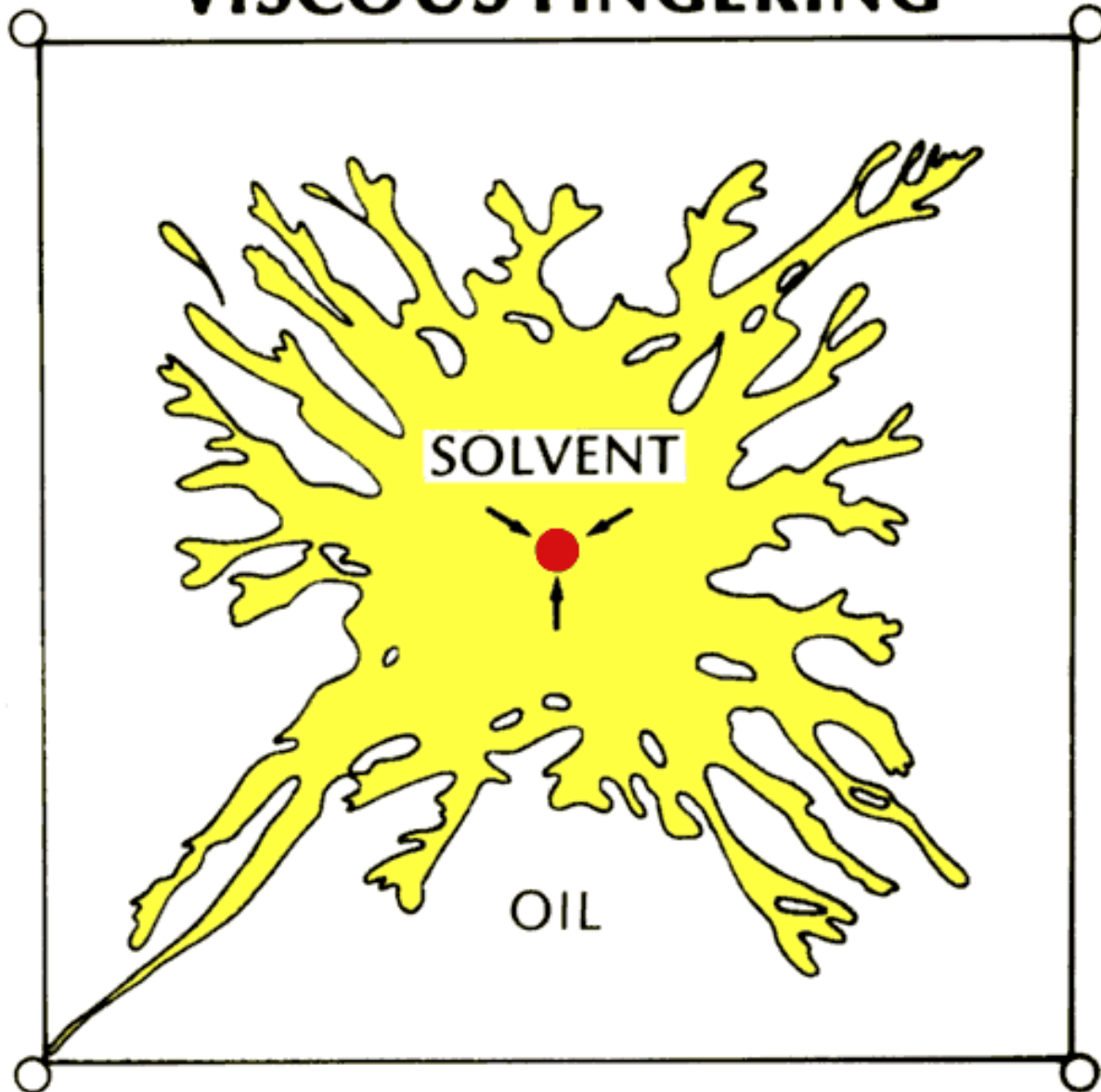




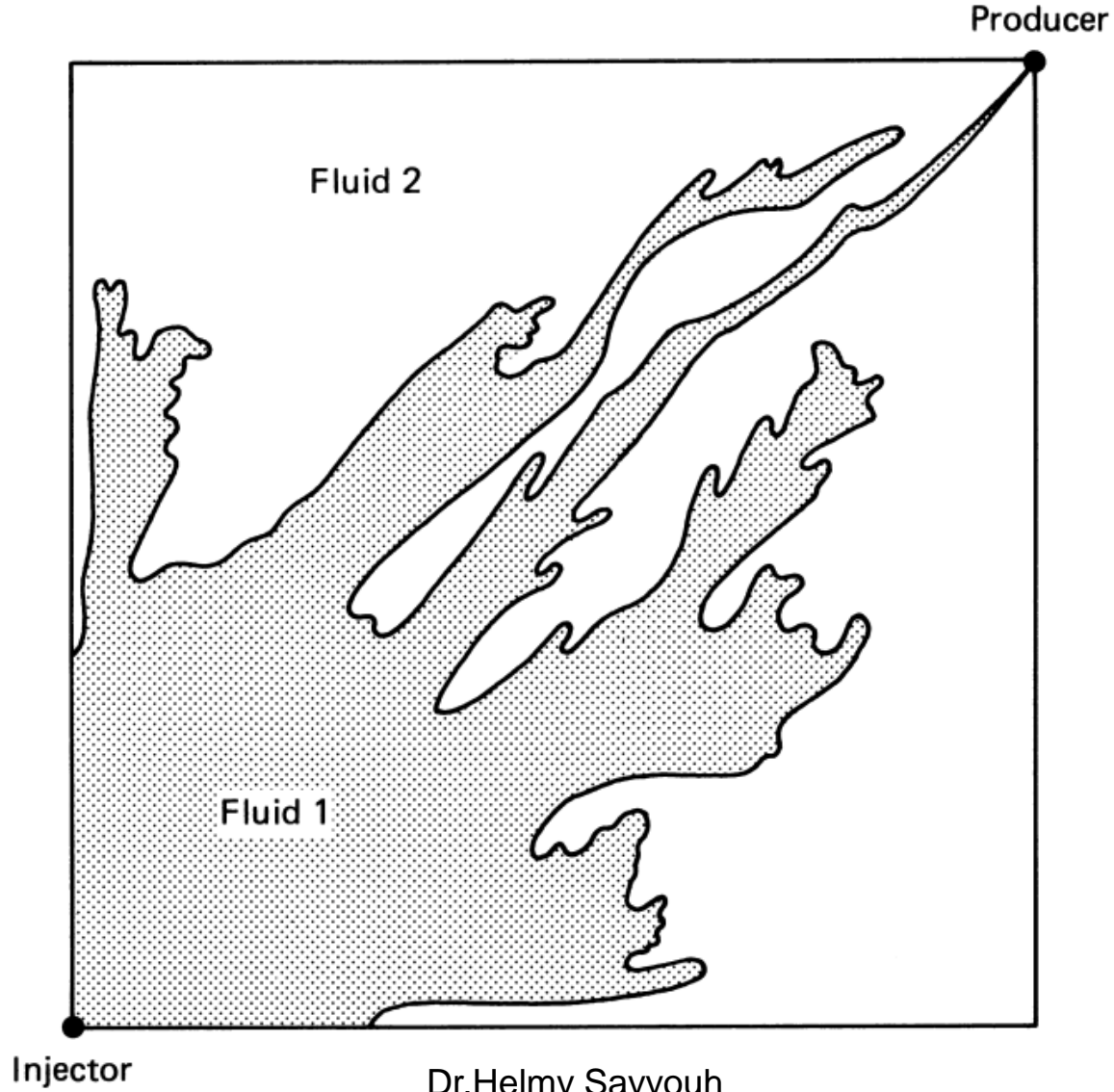
Five-Spot Areal Sweep...



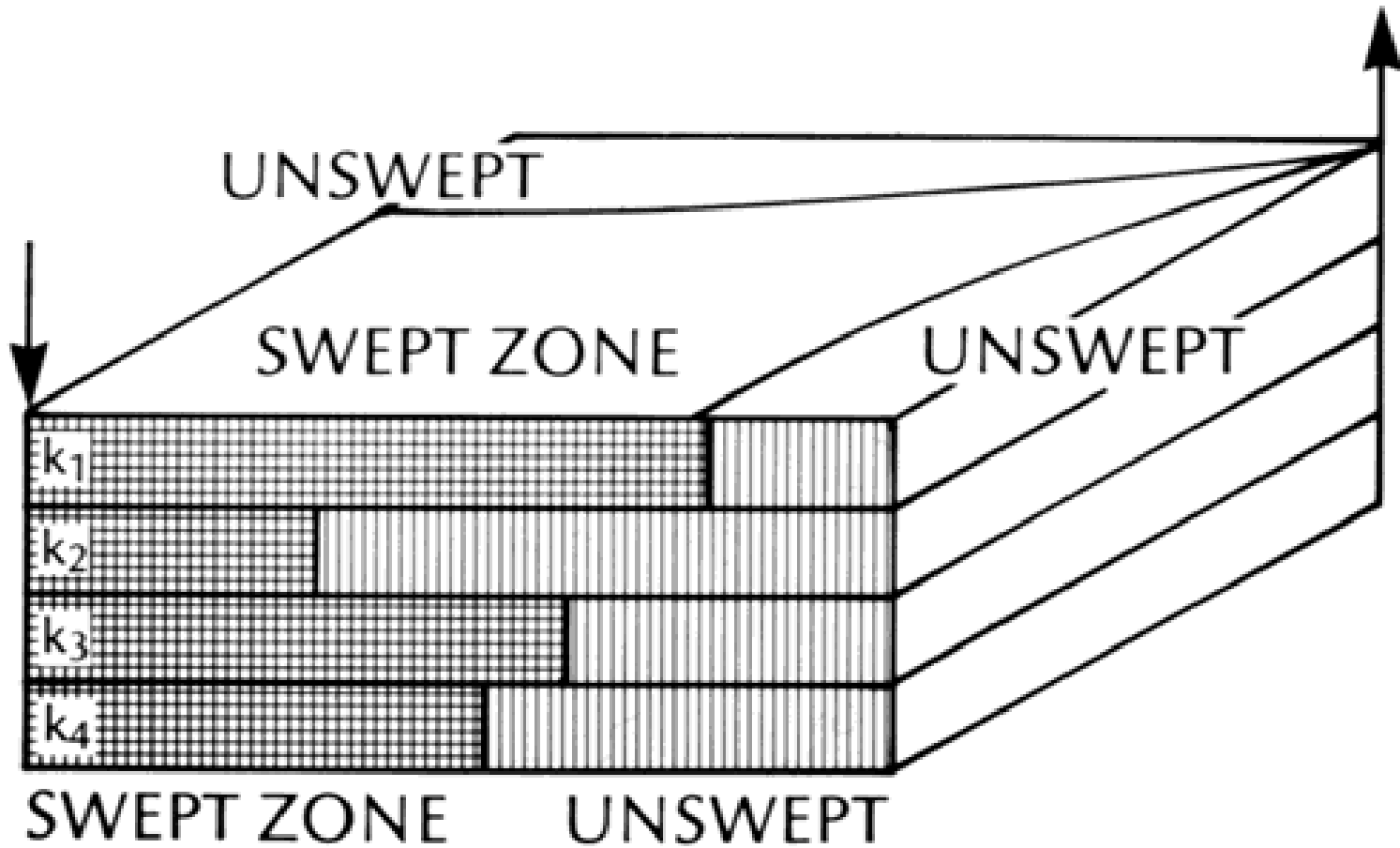
VISCOUS FINGERING



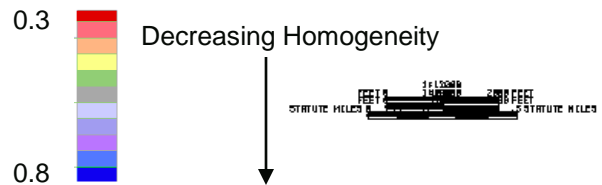
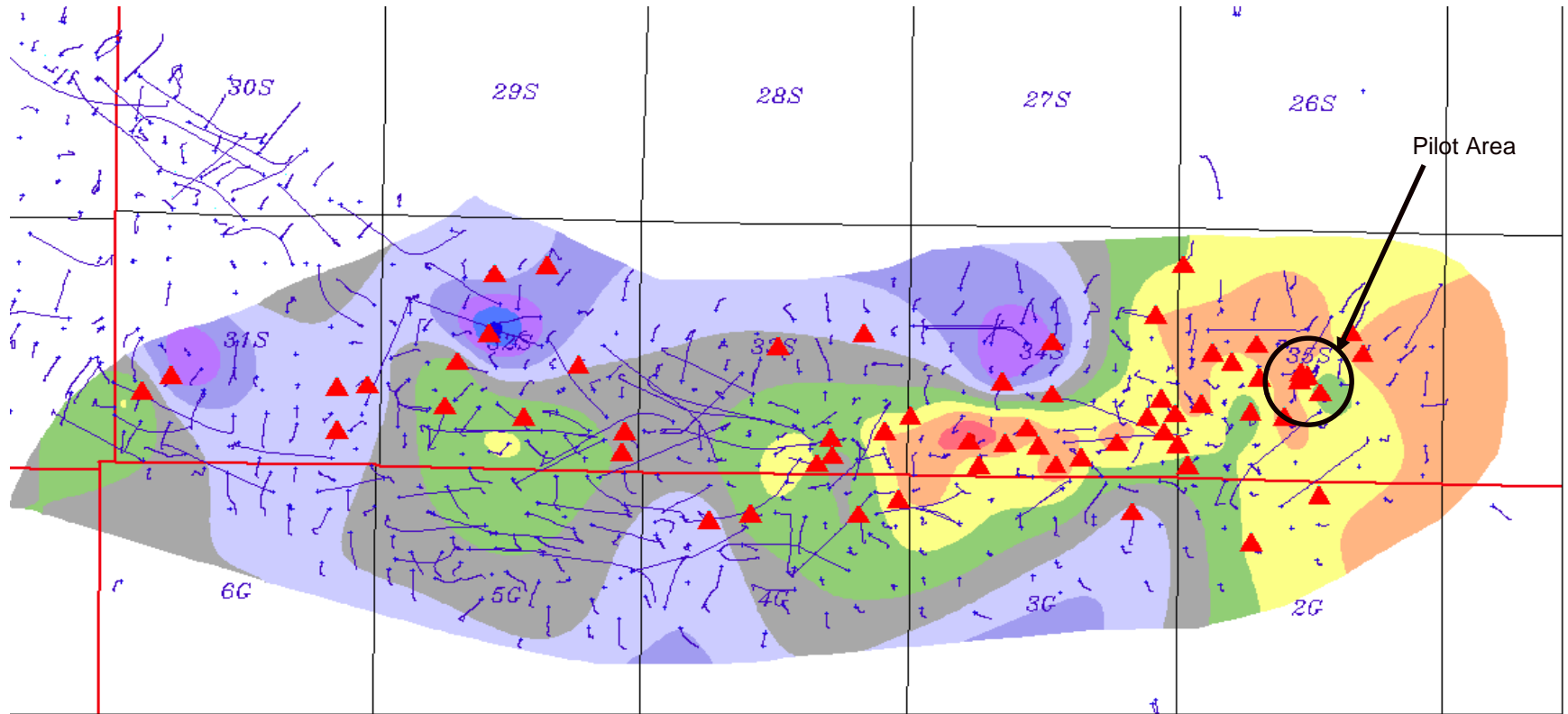
Viscous Fingering in a Quarter Five-spot Model, $M^o = 17$



VERTICAL SWEEP EFFICIENCY

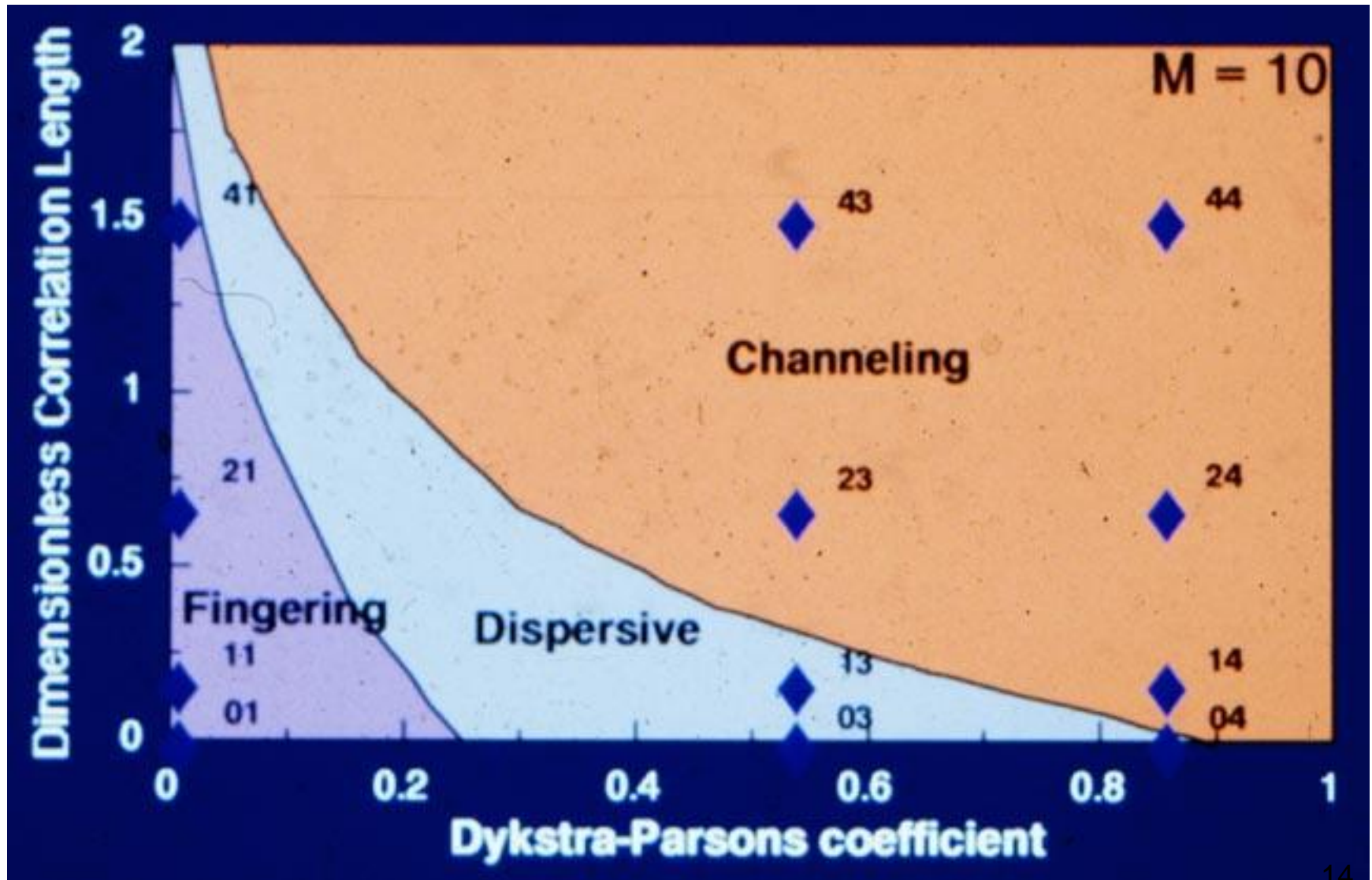


Dykstra Parsons Coefficient Map

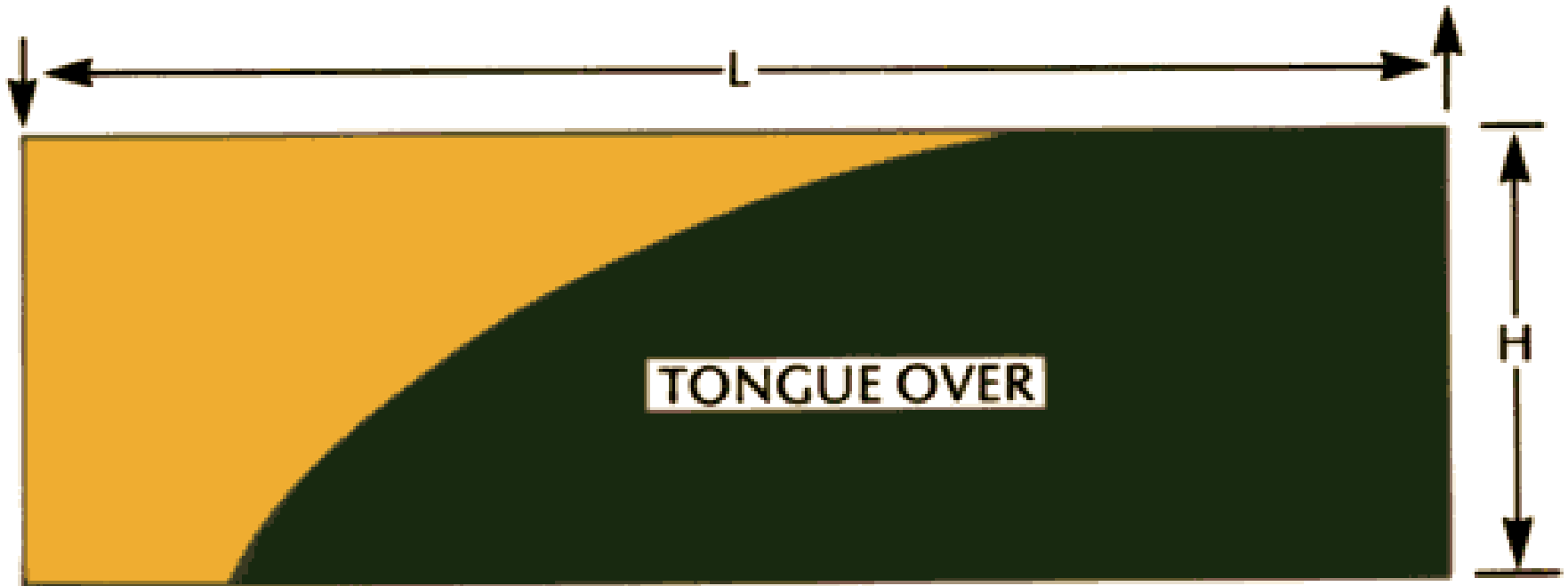


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WATERFLOOD RMT DYKSTRA-PARSONS	
DATE	29-11-2011

Displacement Regime Diagram (M=10)...

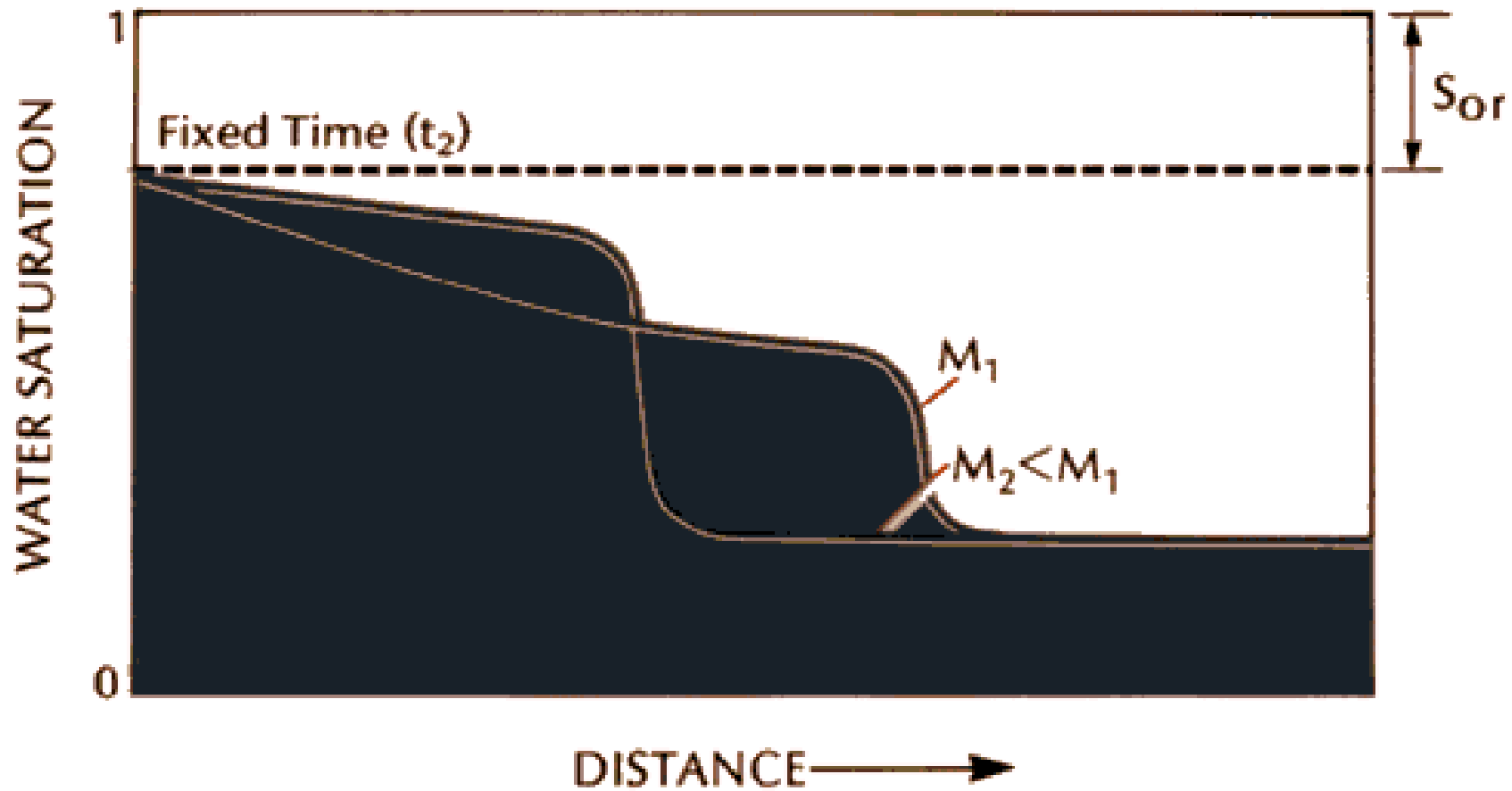


GRAVITY EFFECT



DENSITIES: DISPLACING < DISPLACED
(Gas Displacements)

EFFECT OF MOBILITY RATIO on E_D



Capillary Desaturation Curve...

