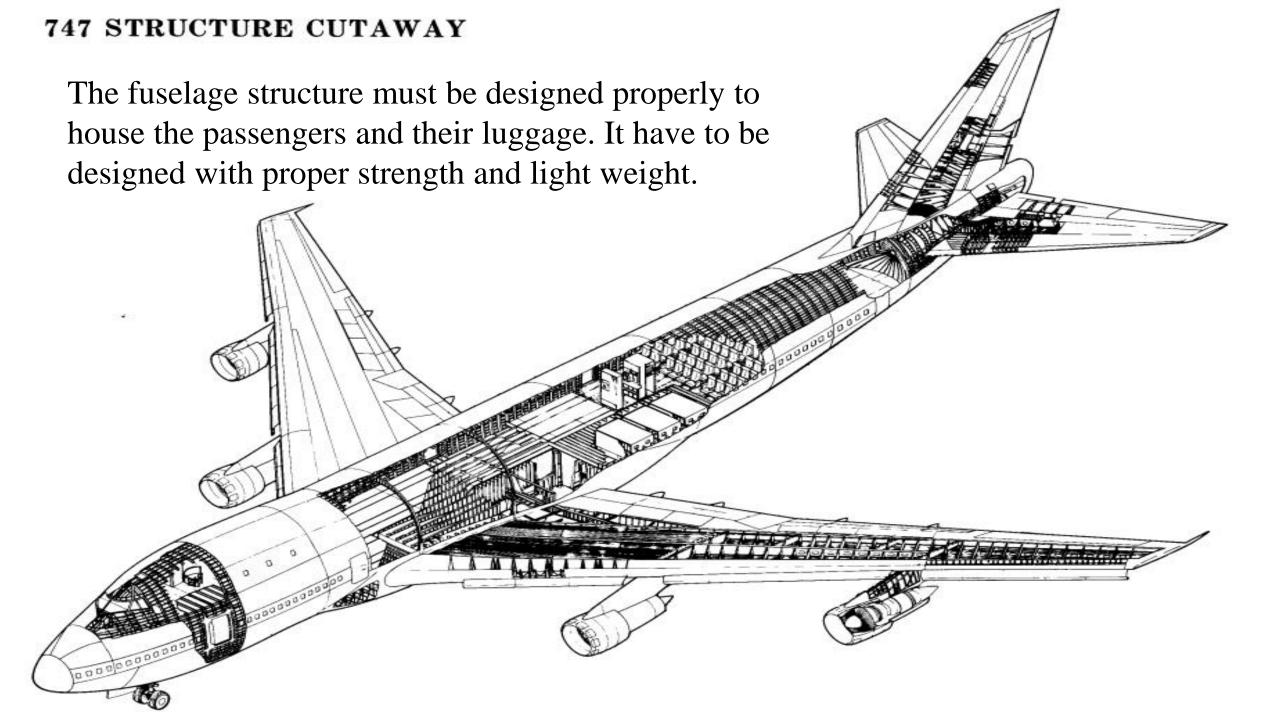
# Airframe Design and Construction

Fuselage Ultimate bending strength

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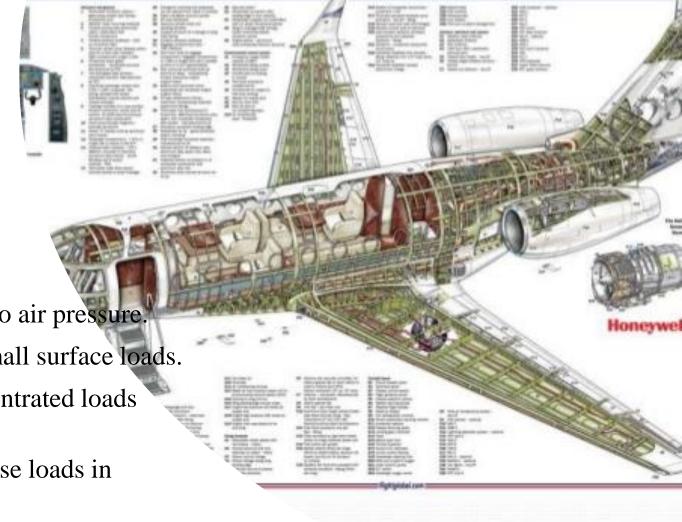
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## Fuselage loads

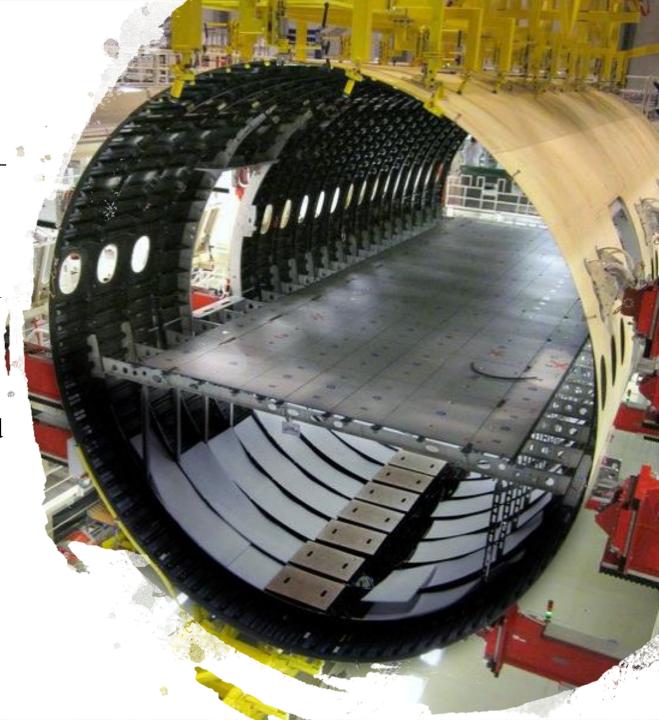
- The wing is subject to large distributed loads due to air pressure.
- ➤ However, the fuselage is subjected to relatively small surface loads.
- The fuselage is subjected to large amount of concentrated loads such as the wing reactions, the landing gear loads.
- The fuselage must be designed to withstand all these loads in addition to the internal pressure.
- ➤ It is found that the best efficient shape to handle all these loads effectively is the circular cross-section.



## Fuselage Structure

#### The fuselage structure is usually

- ➤ a single cell thin walled tube with many transverse frames or rings, and longitudinal stringers.
- rovides combined elements which can handle concentrated and distributed applied loads efficiently and safely.
- ➤ simply is a beam structure subjected to bending, torsional, and axial forces.
- has many cutouts and discontinuity.



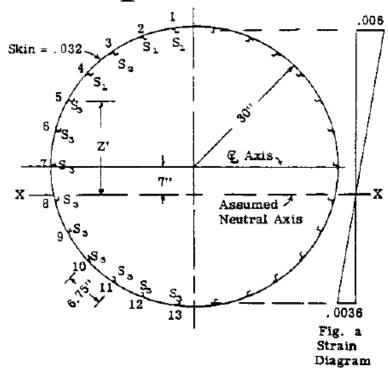
## Fuselage structure analysis

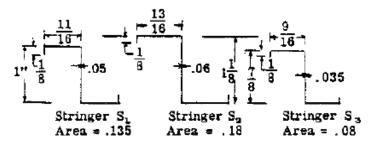
Figure Given fuselage structure and determine the <u>ultimate bending</u> <u>strength</u>.

Figure Given loads and determine the <u>maximum stresses</u> applied to the fuselage structure.

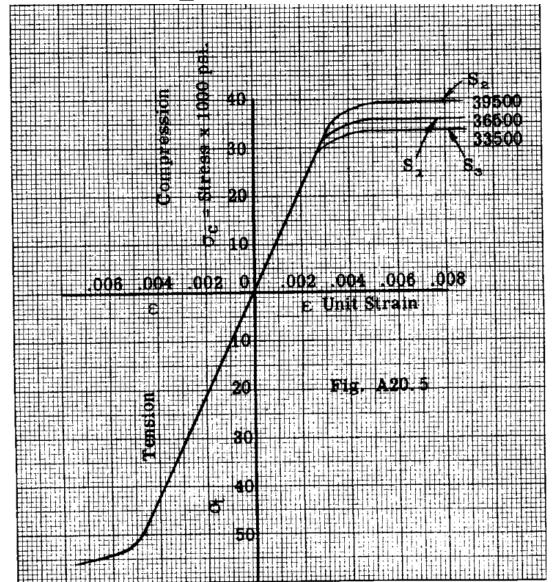
➤ Given loads and determine the *shear flow distribution*.

The figure shows a circular fuselage cross-section. The stringers are arranged symmetrically w.r.t. the fuselage center point. Three stringers are used as illustrated in the Figure. The material is aluminum 2024.





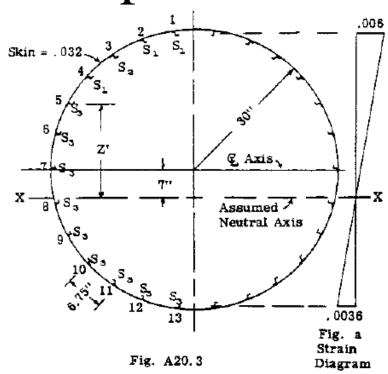
Given the stringers' stress-strain curve, determine the fuselage ultimate bending strength?



#### Solution strategy

- The fuselage is under bending moment which results in compression in the upper portion and tension in the lower portion.
- The location of the centroid in unknown and subsequently the location of the neutral axis.
- Due to symmetry about the z-axis, only half of the fuselage can be considered in the present calculations.
- Neglect the buckled skin effect.
- We will use the beam stress formula which is based on linear stress variation

$$\sigma_b = -\frac{M_\chi z}{I_\chi}$$



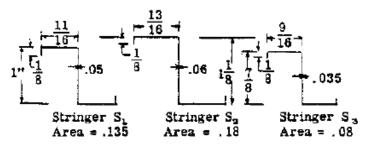
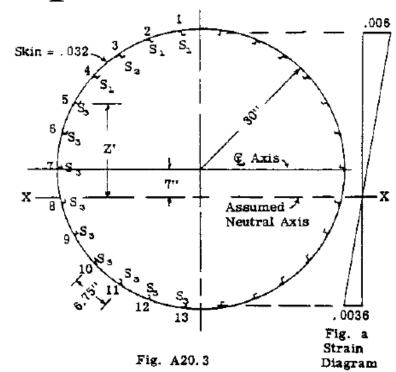


Fig. A20.4

### Solution process

1. List the stringer number, stringer type, and stringer area.

Stringer		Stringer Area
no.	Type	$A_{st}$ [ $in^2$ ]
1	<b>S</b> 1	0.135
2	<b>S</b> 1	0.135
3	S2	0.18
4	<b>S</b> 1	0.135
5	<b>S</b> 3	0.08
6	<b>S</b> 3	0.08
7	<b>S</b> 3	0.08
8	<b>S</b> 3	0.08
9	<b>S</b> 3	0.08
10	<b>S</b> 3	0.08
11	<b>S</b> 3	0.08
12	<b>S</b> 3	0.08
13	<b>S</b> 3	0.08



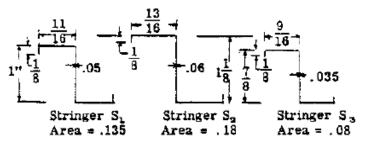
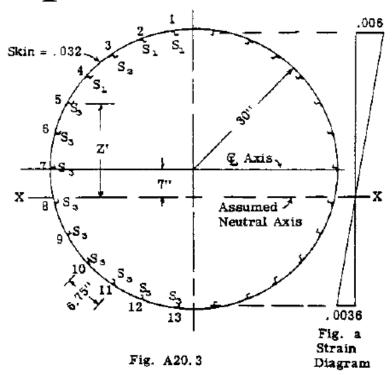


Fig. A20.4

#### Solution process

2. Stringers initial position

Angle	Radius	Initial Centroid
$\theta[rad]$	R [ <i>in</i> ]	Z' [ <i>in</i> ]
1.69163	29.484	36.269
1.93329	29.484	34.568
2.17495	29.4215	31.2134
2.41661	29.484	26.5515
2.65827	29.5465	20.7309
2.89993	29.5465	14.0709
3.14159	29.5465	7
3.38325	29.5465	-0.0709
3.62491	29.5465	-6.7309
3.86658	29.5465	-12.593
4.10824	29.5465	-17.316
4.3499	29.5465	-20.626
4.59156	29.5465	-22.331



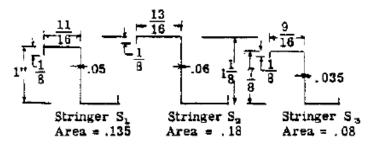


Fig. A20.4

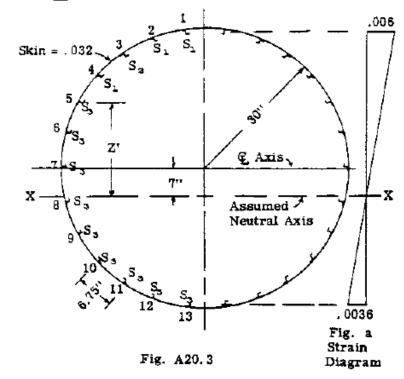
### Solution process

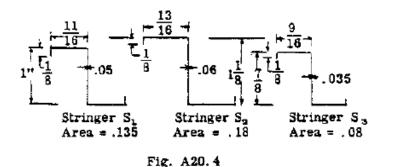
# 2. Effective width and effective area

- Assume linear stress.
- All skin areas in the tension side are effective.

$$w_{eff} = 1.9t \sqrt{\frac{E}{\sigma_{st}}}$$

effective	Total
Area	area
$A_{eff}$ $[in^2]$	$A_{tot} [in^2]$
0.03268	0.16768
0.03348	0.16848
0.03523	0.21523
0.0382	0.1732
0.04323	0.12323
0.05247	0.13247
0.0744	0.1544
0.108	0.188
0.216	0.296
0.216	0.296
0.216	0.296
0.216	0.296
0.216	0.296
	Area $A_{eff} [in^2]$ $0.03268$ $0.03348$ $0.03523$ $0.0382$ $0.04323$ $0.05247$ $0.0744$ $0.108$ $0.216$ $0.216$ $0.216$ $0.216$





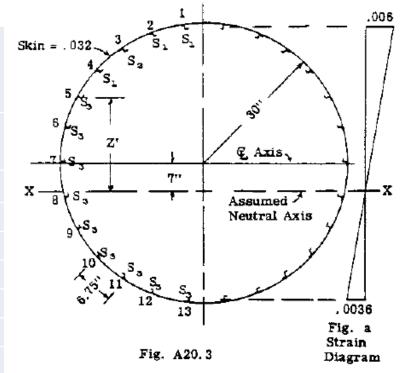
### Solution process

# 3. Nonlinear stress correction

- Correct the linear stress assumption based on the linear strain distribution.
- The true stresses are calculated from the given stress strain relations.

$$K_{eff} = \frac{\sigma_{true}}{\sigma_{linear}}$$

linear strain	True stress	Effective correction factor	Corrected Effective Area
$arepsilon_{linear}$	σ <sub>true</sub> [psi]	$K_{eff}$	$A_{corr}$
-0.006	-36500	1	0.1677
-0.005719	-36500	1.0492	0.1768
-0.005164	-39100	1.2447	0.2679
-0.004392	-36000	1.34727	0.2333
-0.003430	-31500	1.50985	0.1861
-0.002328	-24000	1.6948	0.2245
-0.001158	-12500	1.774	0.2740
0.000012	0	1	0.1880
0.001114	10000	1.476	0.4370
0.002083	20500	1.617	0.4788
0.002865	30000	1.721	0.5096
0.003412	35000	1.686	0.4991
0.003694	38000	1.69	0.5005
			4.1432



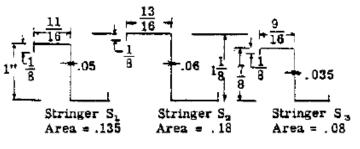


Fig. A20.4

#### Solution process

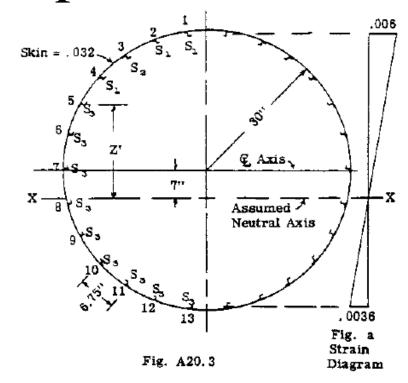
4. First moment of area, centroid, and second moment of area.

$$\bar{Z} = \frac{\sum A_{corr} Z'}{\sum A_{corr}} = \frac{-3.59}{4.143} = -0.87 \ in$$

$$Z = Z' - \bar{Z}$$

$$I_{xx} = 2\sum A_{corr}Z^2 = 3405 \ in^4$$

First moment	Centroid	Second moment of
of area		area
$A_{corr}Z'$	Z	$A_{corr}Z^2$
6.08171	37.1367	231.258
6.11052	35.4357	221.966
8.36227	32.0811	275.728
6.1957	27.4192	175.433
3.85718	21.5986	86.7966
3.15922	14.9386	50.1046
1.91773	7.86768	16.9583
-0.0133	0.79674	0.11934
-2.9413	-5.8633	15.0224
-6.0296	-11.725	65.8275
-8.8238	-16.449	137.867
-10.294	-19.759	194.849
-11.177	-21.463	230.572
-3.5949		1702.5



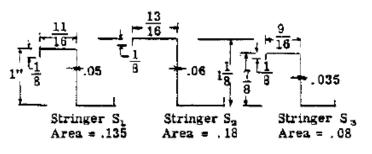
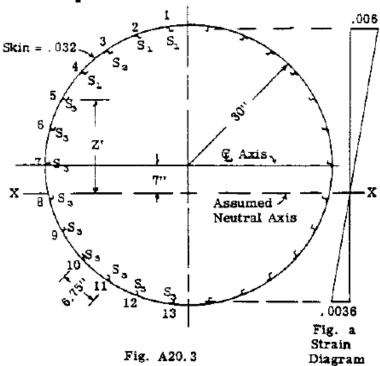


Fig. A20.4

### Solution process

5. Fuselage ultimate bending strength.

$$M_x = -\frac{\sigma_b I_x}{z} = \frac{36500 * 3405}{37.1367} = 3.335 \text{ E6 Ib.in}$$



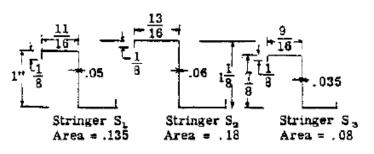
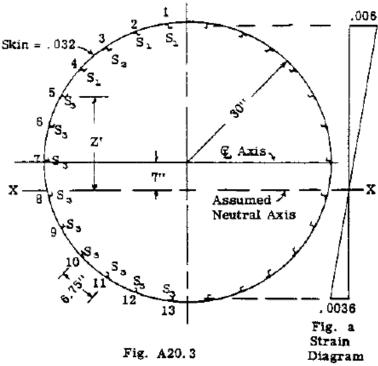


Fig. A20.4

#### **Comments**

- Although the arm of stringer 3 is smaller than that of stringer 1, stringer 3 carries more stresses than stringer 1 and 2.
- The stress distribution is assumed to be linear, since the bending stress equation is based on linear stress analysis.
- The ultimate bending strength is a property to the structure which is independent to the applied loads.



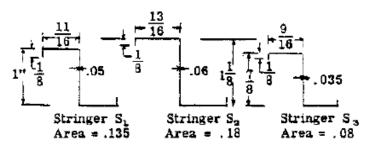


Fig. A20.4

#### **Comments**

• The nonlinear stress effect is important

What will happen if the nonlinear stress effect was not considered?

