

Faraday's Law Applications

1

1. Inductors.
2. Transformers.
3. Electrical Generators.
4. Electrical Motors.
5. Transmission Lines.

Motors: *DC Motor*

2



THE UNIVERSITY OF NEW SOUTH WALES

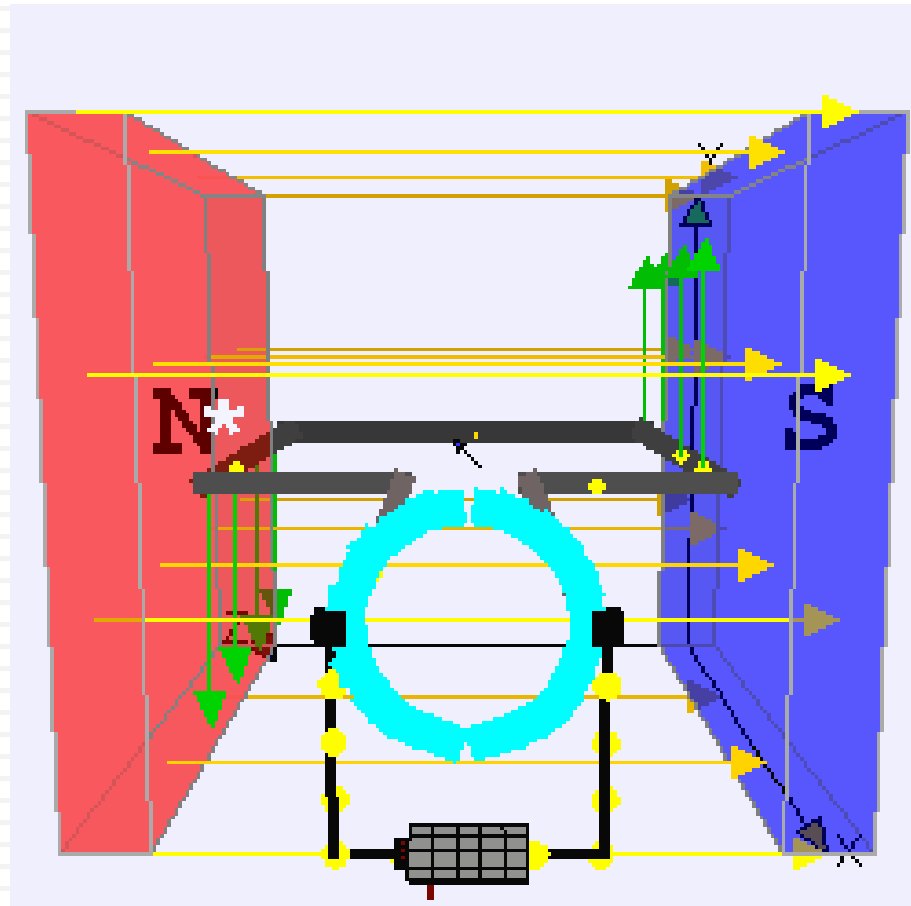
- ▶ play
- ◻ stop
- ▶▶ step
- ◀◀ rew



from PHYSCLIPS

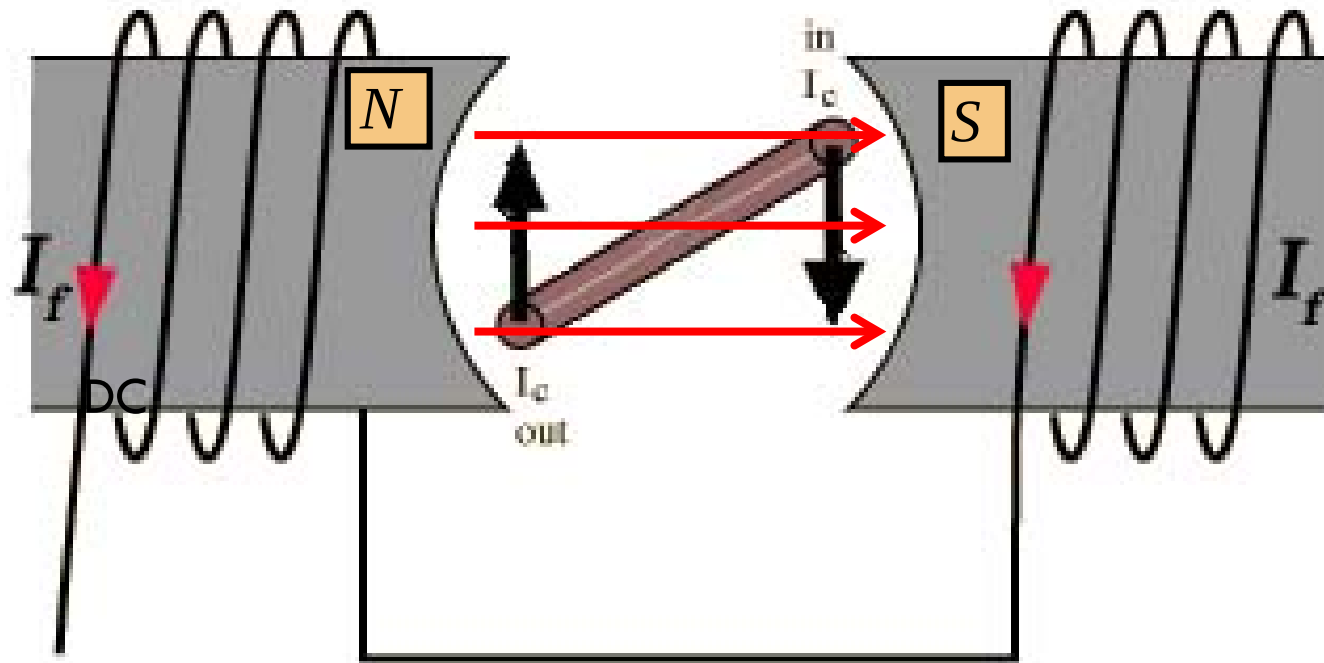
Motors: *DC Motor*

3



Motors: *DC Motor*

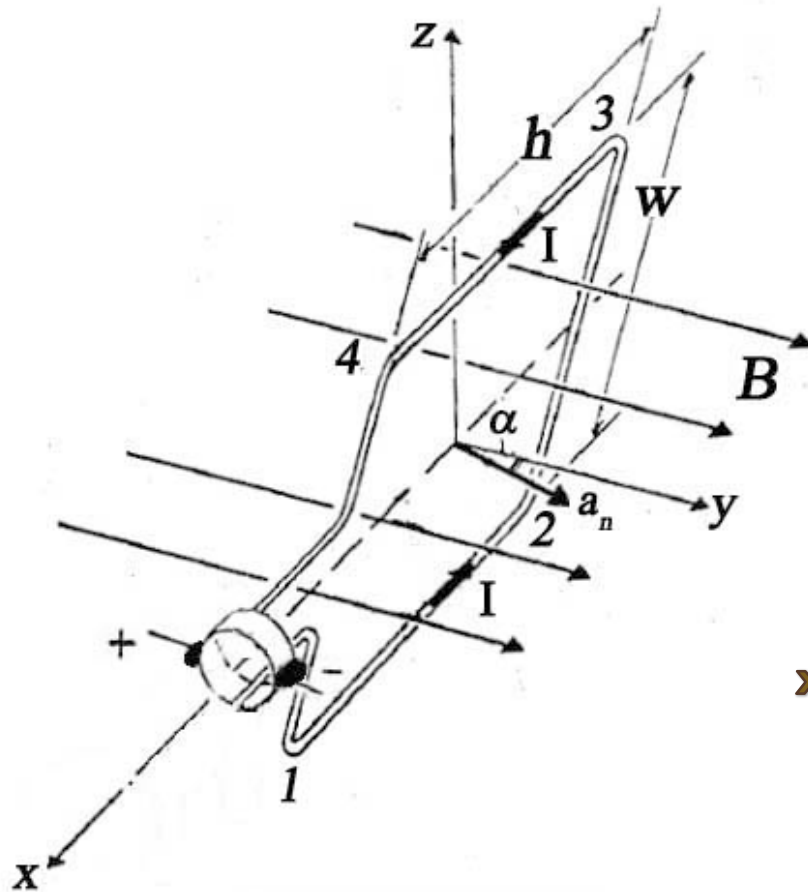
4



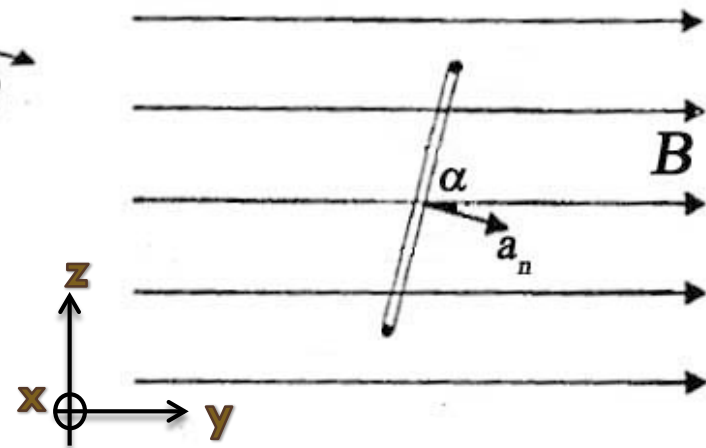
$$B = B_o$$

Motors: *DC Motor*

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(a) Perspective View



(b) View from $+x$ direction

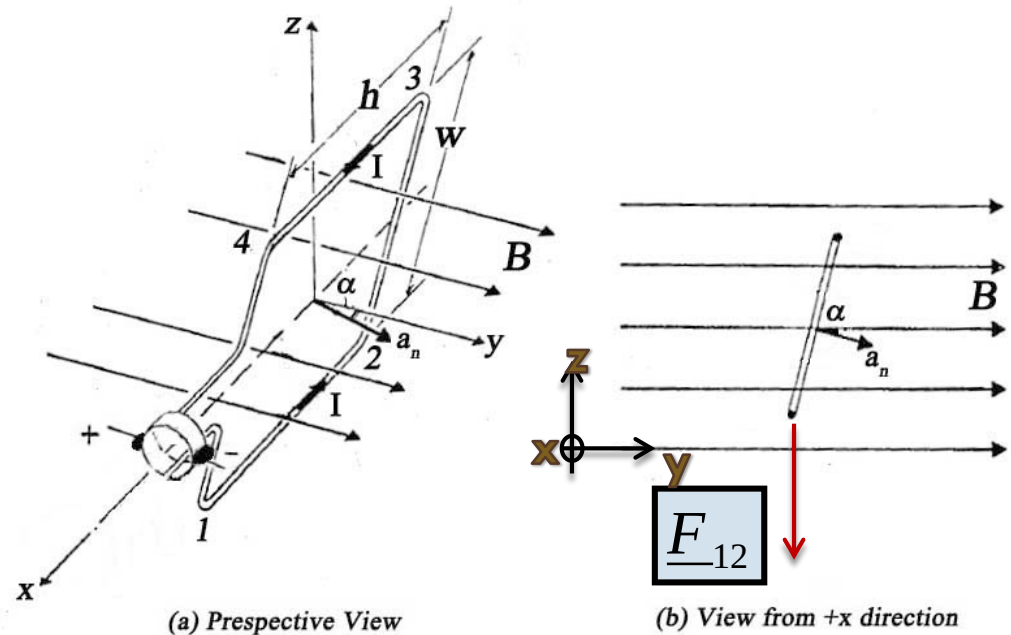
Motors: *DC Motor*

6

$$\underline{F}_m = I \int \underline{dl} \times \underline{B}$$

$$\underline{F}_{12} = I \int_1^2 \underline{dl} \times \underline{B}$$

$$\underline{B} = B_o \underline{u}_y$$



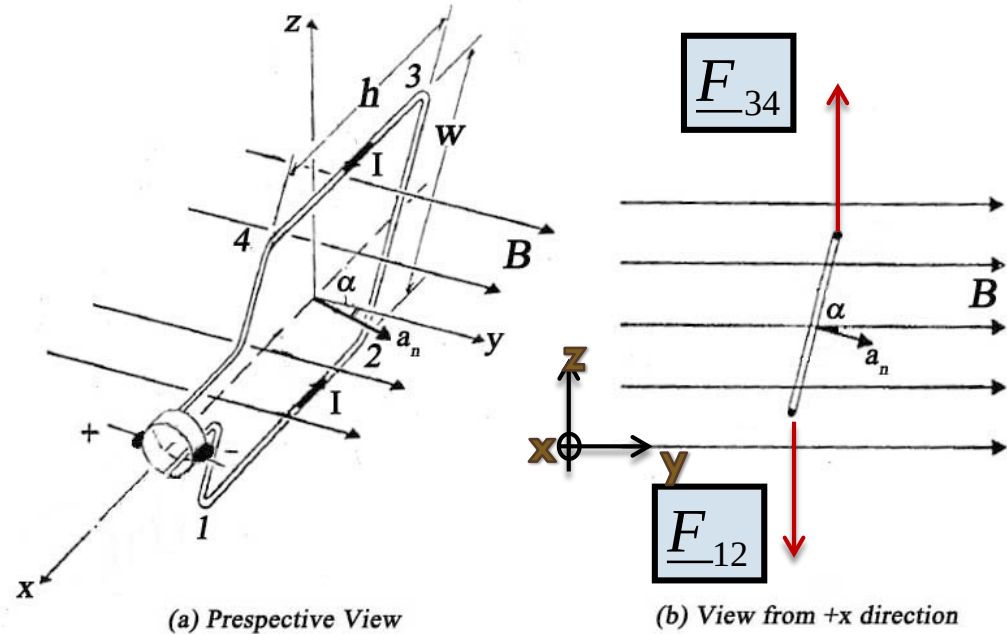
$$\underline{F}_{12} = I \int_{1=0}^{2=h} dx (-\underline{u}_x) \times B_o \underline{u}_y$$

$$\underline{F}_{12} = IB_o h (-\underline{u}_z)$$

Motors: *DC Motor*

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$$\underline{F}_{34} = I \int_3^4 \underline{dl} \times \underline{B}$$



$$\underline{F}_{34} = I \int_{3=0}^{4=h} dx (\underline{u}_x) \times B_o \underline{u}_y$$

$$\underline{F}_{12} = IB_o h (\underline{u}_z)$$

Motors: *DC Motor*

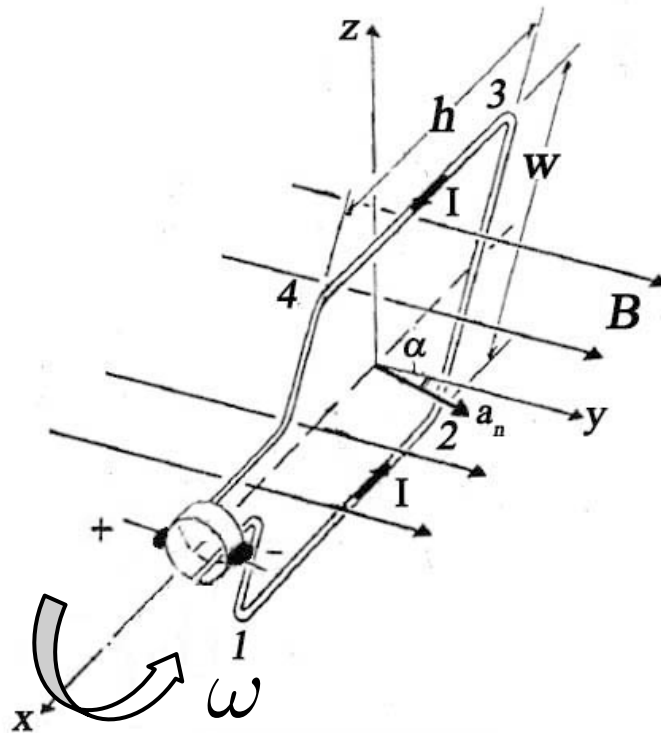
8

$$\underline{T} = \underline{r} \times \underline{F}$$

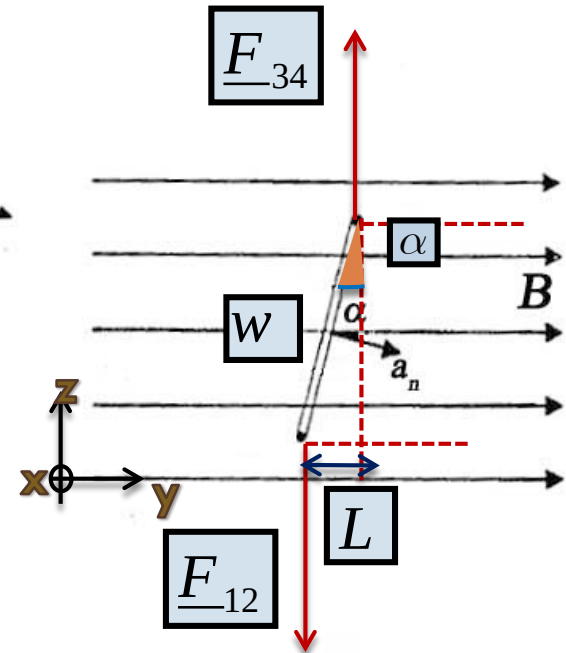
$$T = FL$$

$$L = w \sin \alpha$$

$$F = IB_o h$$



(a) Perspective View



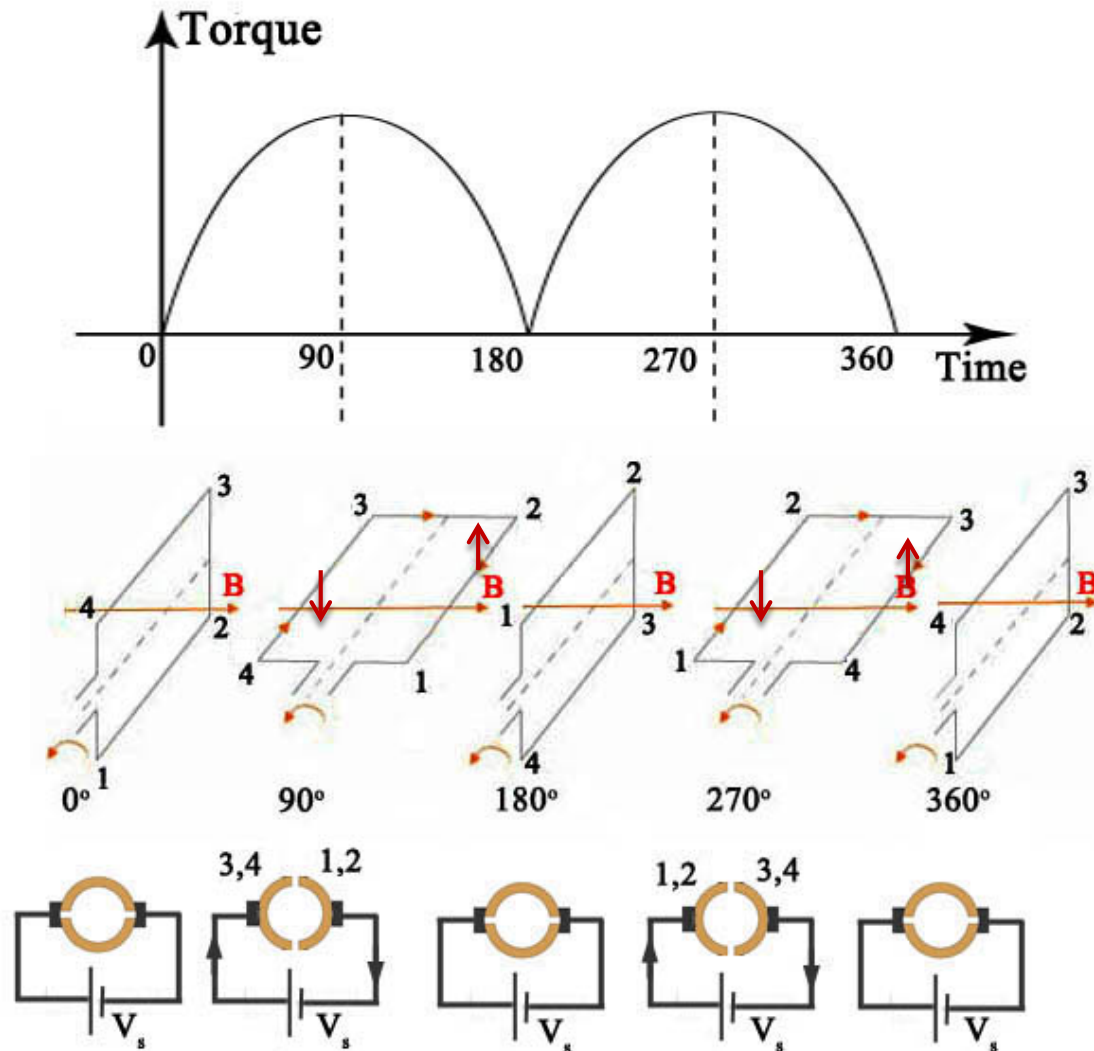
(b) View from +x direction

$$T = IB_o (hw) \sin \alpha$$

$$T = IB_o (hw) \sin(\omega t)$$

Motors: *DC Motor*

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Motors: *DC Motor*

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$$\underline{T} = \underline{m} \times \underline{B}$$

$$\underline{m} = I \underline{S}$$

$$\underline{m} = I (hw) \underline{a}_n$$

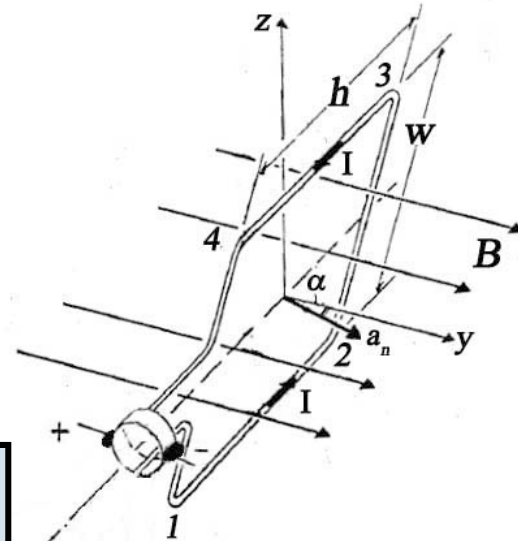
$$\underline{T} = I (hw) \underline{a}_n \times B_o \underline{u}_y$$

$$\underline{T} = IB_o A \sin \alpha (\underline{u}_x)$$

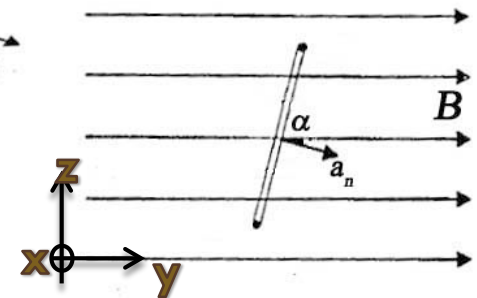
$$P_m = T \omega$$

$$P_m = \omega IB_o A \sin \alpha$$

$$\underline{a}_n \times \underline{u}_y = (1)(1) \sin \alpha (\underline{u}_x)$$



(a) Perspective View

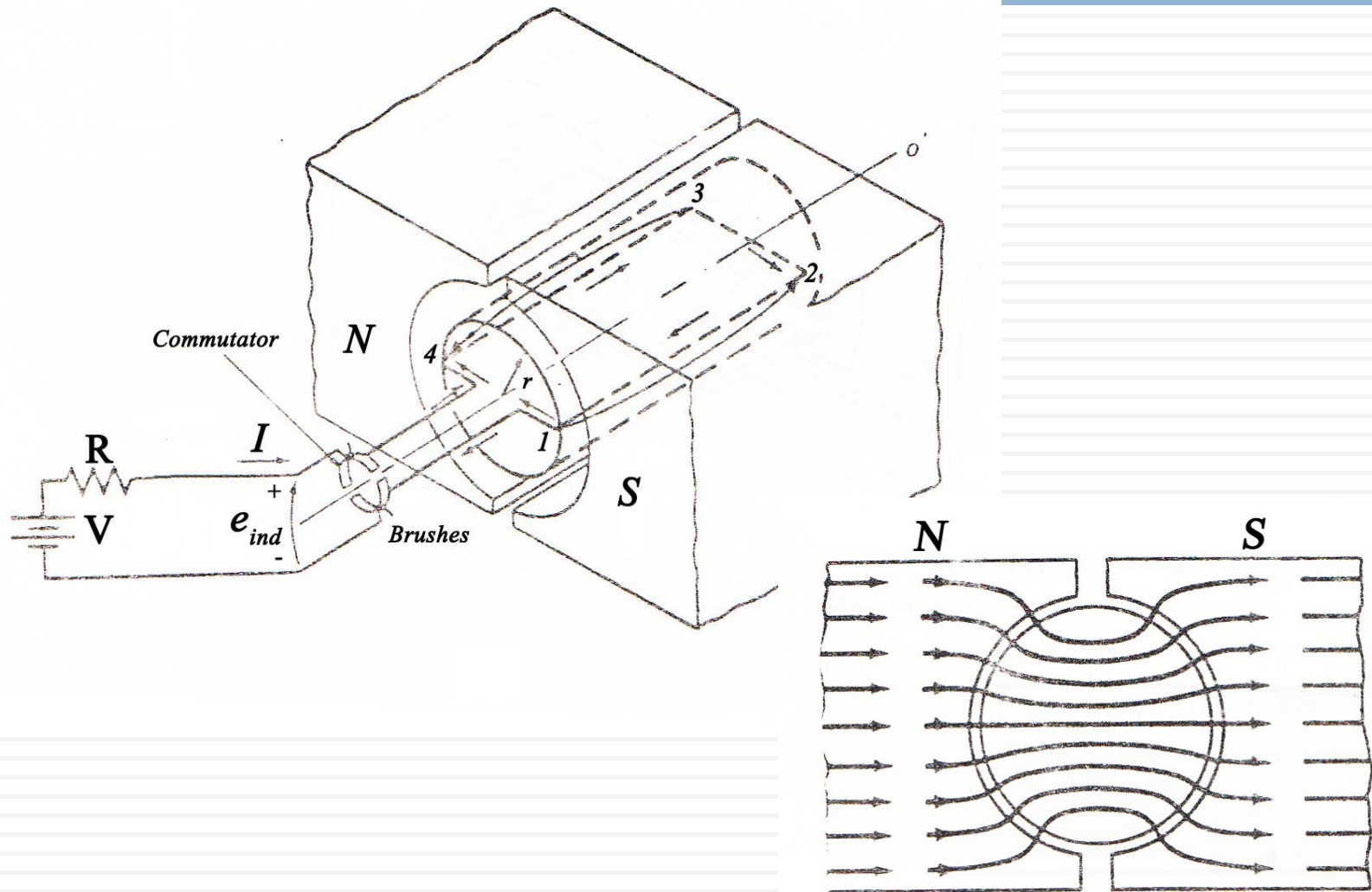


(b) View from $+x$ direction

$$A = hw$$

Motors: **DC Motor**

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Motors: *DC Motor*

12

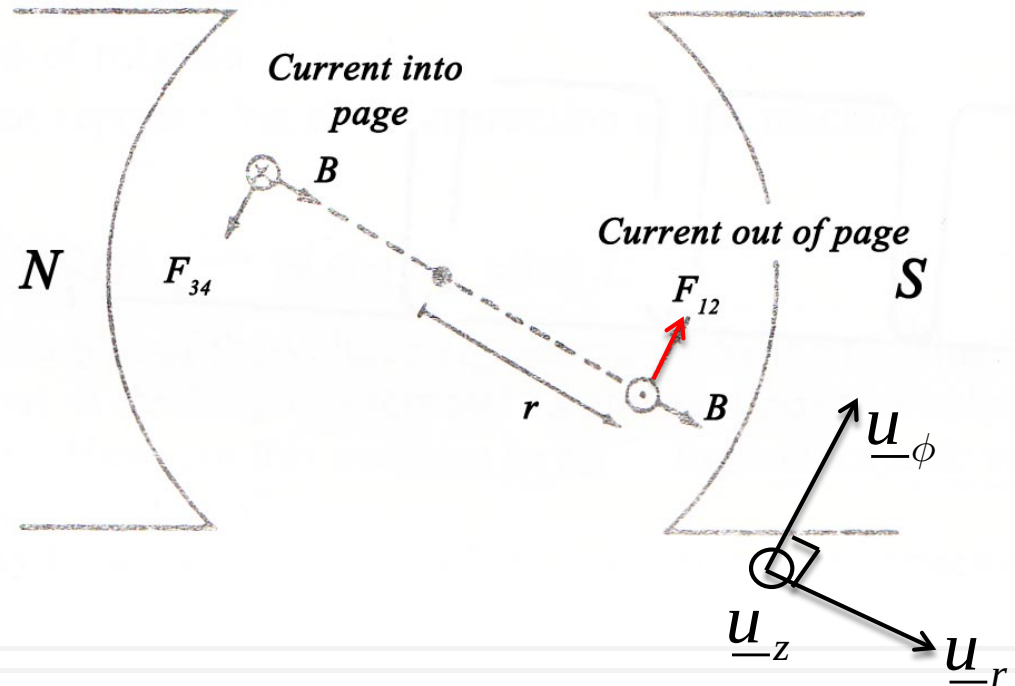
$$\underline{F}_m = I \int \underline{dl} \times \underline{B}$$

$$\underline{F}_{12} = I \int_1^2 \underline{dl} \times \underline{B}$$

$$\underline{B} = B_o \underline{u}_r$$

$$\underline{F}_{12} = I \int_{1=0}^{2=h} dz (\underline{u}_z) \times B_o \underline{u}_r$$

$$\underline{F}_{12} = IB_o h(\underline{u}_\phi)$$

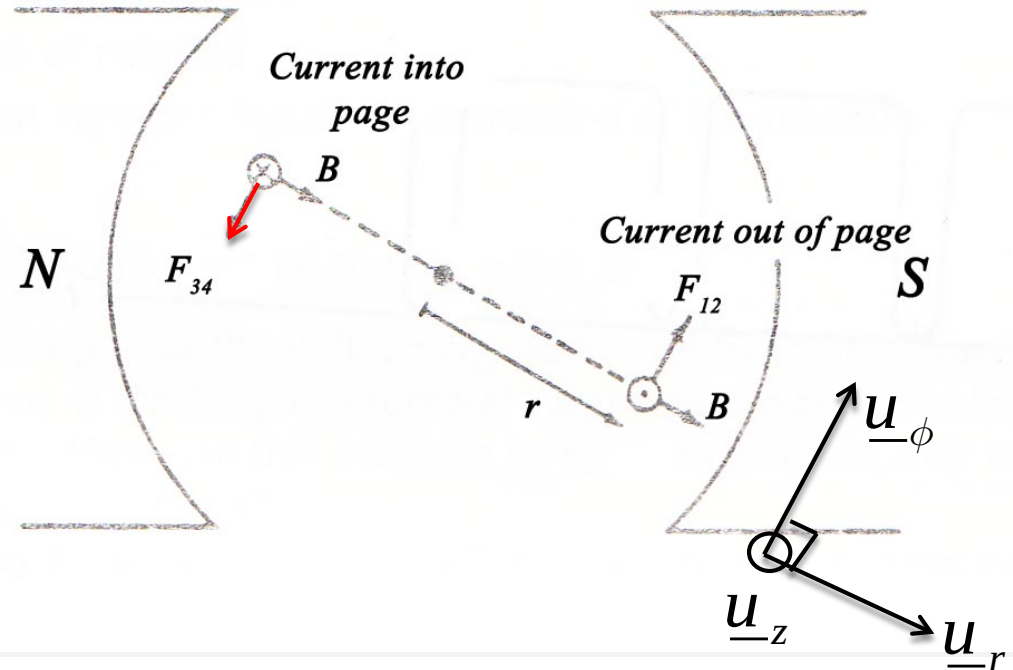


Motors: *DC Motor*

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$$\underline{F}_{34} = I \int_3^4 \underline{dl} \times \underline{B}$$

$$\underline{B} = B_o (-\underline{u}_r)$$

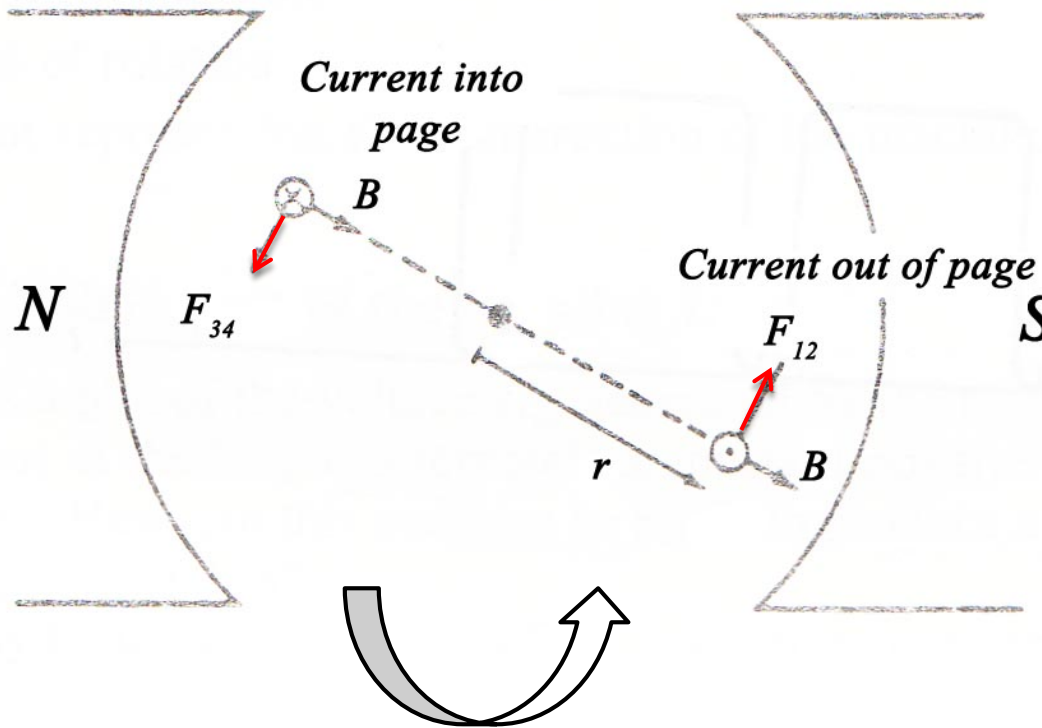


$$\underline{F}_{34} = I \int_{3=0}^{4=h} dz (-\underline{u}_z) \times B_o (-\underline{u}_r)$$

$$\underline{F}_{34} = IB_o h (\underline{u}_\phi)$$

Motors: *DC Motor*

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Motors: *DC Motor*

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$$\underline{T} = \underline{r} \times \underline{F}$$

$$T = FL$$

$$T = (2r)IB_o h$$

➔ $T = 2IB_o(rh)$

Under the pole faces

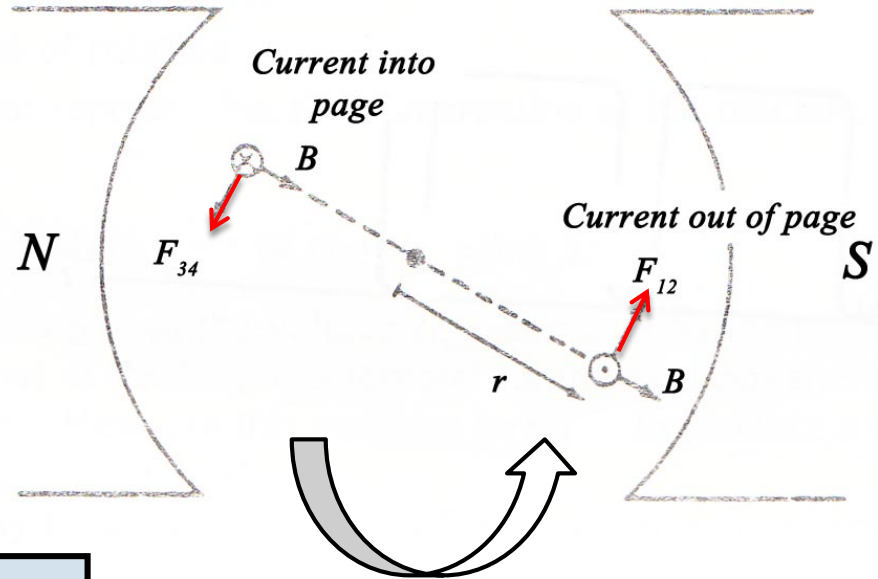
$$T = 0$$

Beyond the pole edges

➔ $T = \frac{2}{\pi} A_p B_o I$

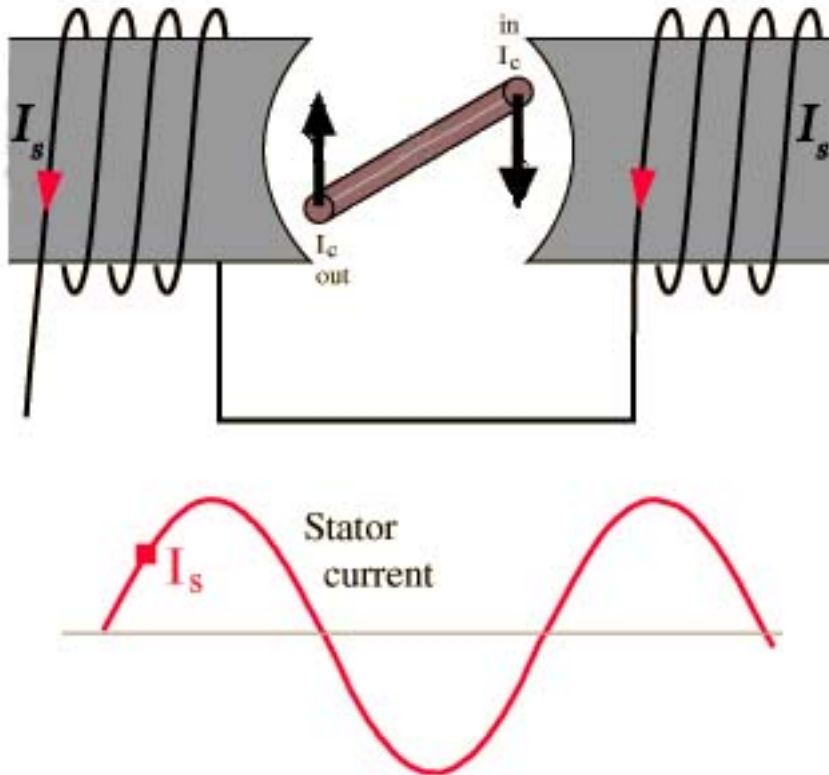
➔ $T = \frac{2}{\pi} \phi I$

ϕ = Total flux under one pole



Motors: *AC Motor*

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$$B = B_o \sin \omega_1 t$$

$$\omega_1 = 2\pi f$$

Motors: AC Motor

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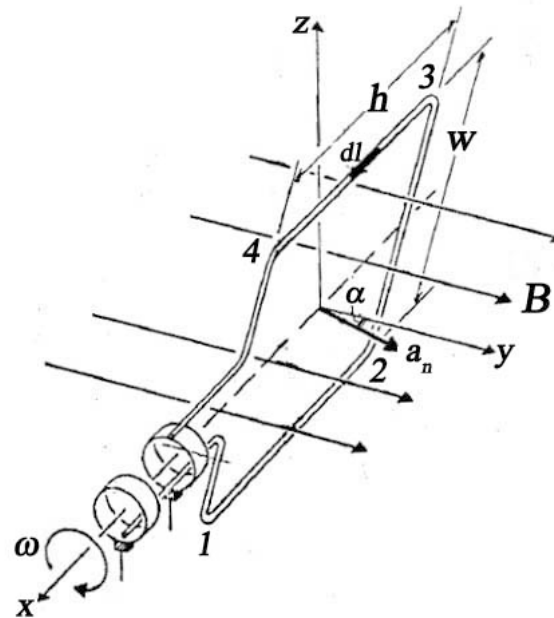
$$e = - \int_s \frac{\partial \underline{B}}{\partial t} \cdot d\underline{S} + \oint_c \underline{v} \times \underline{B} \cdot d\underline{l}$$

$$\underline{B} = B_o \sin \omega_1 t \underline{u}_y$$

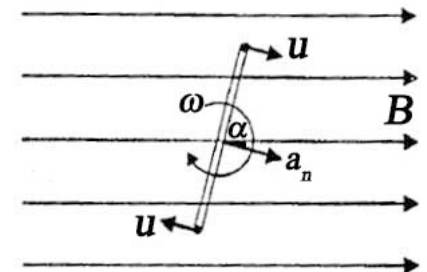
$$e = e_1 + e_2$$

$$e_1 = - \int_s \frac{\partial \underline{B}}{\partial t} \cdot d\underline{S}$$

$$e_1 = - \int_{S=hw} \omega_1 B_o \cos(\omega_1 t) \underline{u}_y \cdot d\underline{S} \underline{a}_n$$



(a) Perspective View



(b) View from +x direction

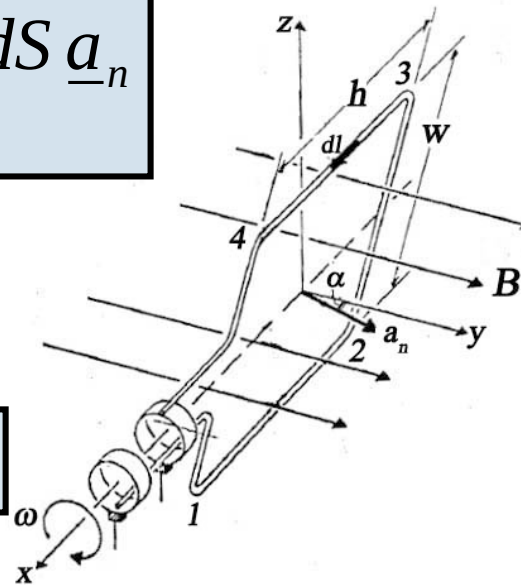
Motors: AC Motor

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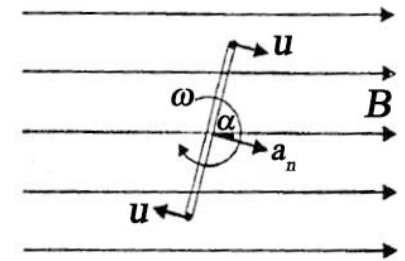
$$e_1 = - \int_{S=wh} \omega_1 B_o \cos(\omega_1 t) \underline{u}_y \cdot d\underline{S} \underline{a}_n$$

$$\underline{a}_n \cdot \underline{u}_y = (1)(1) \cos \alpha$$

$$e_1 = -\omega_1 B_o (wh) \cos(\omega_1 t) \cos(\alpha)$$



(a) Perspective View



(b) View from +x direction

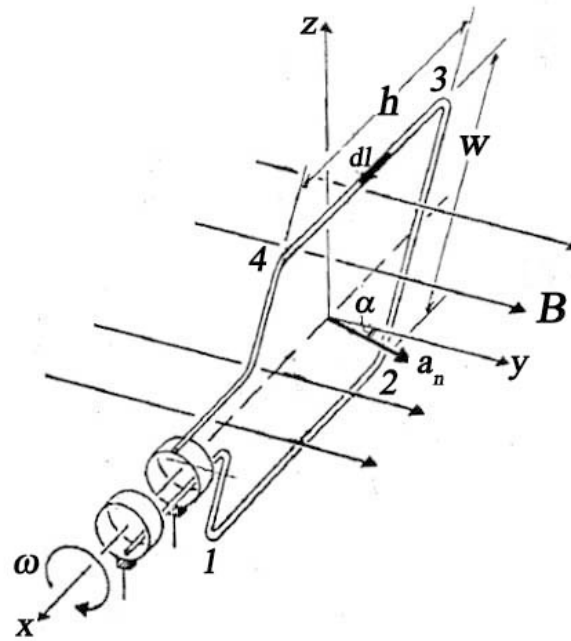
$$e_1 = -\omega_1 B_o (wh) \cos(\omega_1 t) \cos(\omega t + \theta_o)$$

$$e_1 = -\omega_1 B_o \frac{A}{2} [\cos((\omega_1 - \omega)t - \theta_o) + \cos((\omega_1 + \omega)t + \theta_o)]$$

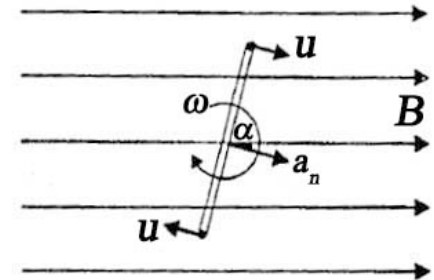
Motors: AC Motor

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$$e_2 = \oint_C \underline{v} \times \underline{B} \cdot d\underline{l}$$



(a) Perspective View



(b) View from $+x$ direction

$$e_2 = \omega B_o (wh) \sin(\omega_1 t) \sin(\omega t + \theta_o)$$

$$e_2 = \omega B_o \frac{A}{2} [\cos((\omega_1 - \omega)t - \theta_o) - \cos((\omega_1 + \omega)t + \theta_o)]$$

Motors: *AC Motor*

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$$e = e_1 + e_2$$

$$e_1 = -\omega_1 B_o \frac{A}{2} [\cos((\omega_1 - \omega)t - \theta_o) + \cos((\omega_1 + \omega)t + \theta_o)]$$

$$e_2 = \omega B_o \frac{A}{2} [\cos((\omega_1 - \omega)t - \theta_o) - \cos((\omega_1 + \omega)t + \theta_o)]$$



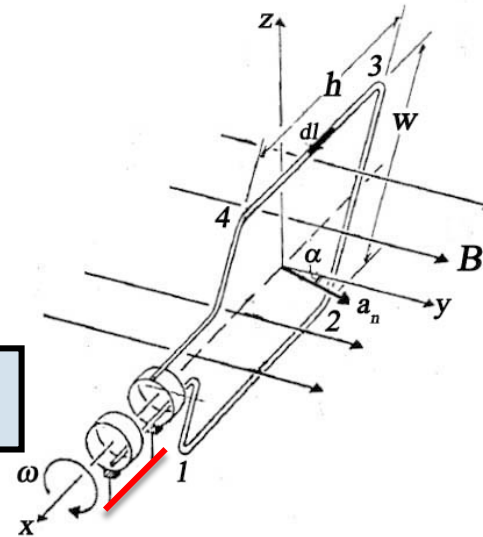
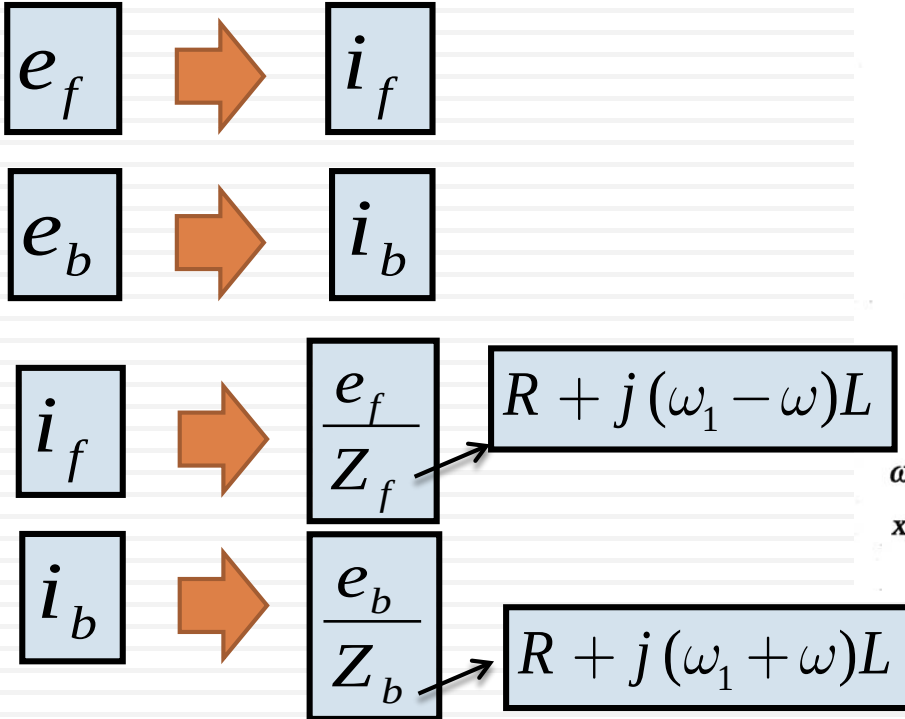
$$e = -B_o \frac{A}{2} [(\omega_1 - \omega) \cos((\omega_1 - \omega)t - \theta_o) + (\omega_1 + \omega) \cos((\omega_1 + \omega)t + \theta_o)]$$



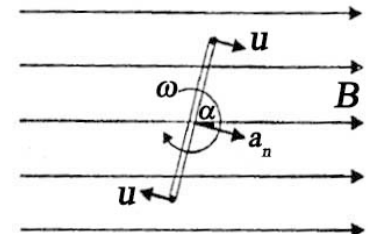
$$e = e_f + e_b$$

Motors: *AC Motor*

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(a) *Prespective View*



(b) View from +x direction

$$i_f = \frac{B_o A}{2|Z_f|} [(\omega_1 - \omega) \cos((\omega_1 - \omega)t - \theta_o - \phi_f)]$$

$$i_b = \frac{B_o A}{2|Z_b|} [(\omega_1 + \omega) \cos((\omega_1 + \omega)t + \theta_o - \phi_b)]$$

Motors: *AC Motor*

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$$i_f = I_{fm} \cos((\omega_1 - \omega)t - \theta_o - \phi_f)$$

$$i_b = I_{bm} \cos((\omega_1 + \omega)t + \theta_o - \phi_b)$$

Torque

$$T_f = \underline{m} \times \underline{B}$$

$$\underline{m} = i_f \underline{S}$$

$$\underline{B} = B_o \sin \omega_1 t \underline{u}_y$$

$$T_f = I_{fm} \cos((\omega_1 - \omega)t - \theta_o - \phi_f) (A \underline{a}_n) \times B_o \sin \omega_1 t \underline{u}_y$$

$$T_f = I_{fm} B_o A \cos((\omega_1 - \omega)t - \theta_o - \phi_f) \sin \omega_1 t \sin(\omega t + \theta_o)$$

$$\sin \omega_1 t \sin(\omega t + \theta_o) = \frac{1}{2} [\cos((\omega_1 - \omega)t - \theta_o) - \cos((\omega_1 + \omega)t + \theta_o)]$$

Motors: *AC Motor*

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Torque

$$T_f = \frac{I_{fm} B_o A}{2} \cos((\omega_1 - \omega)t - \theta_o - \phi_f) \\ * [\cos((\omega_1 - \omega)t - \theta_o) - \cos((\omega_1 + \omega)t + \theta_o)]$$

$$\cos((\omega_1 - \omega)t - \theta_o - \phi_f) * \cos((\omega_1 - \omega)t - \theta_o) = \\ \frac{1}{2} [\cos \phi_f + \cos[2((\omega_1 - \omega)t - \theta_o) - \phi_f]]$$

$$\cos((\omega_1 - \omega)t - \theta_o - \phi_f) * \cos((\omega_1 + \omega)t + \theta_o) = \\ \frac{1}{2} [\cos[2(\omega t + \theta_o) + \phi_f] + \cos(2\omega_1 t - \phi_f)]$$

Motors: *AC Motor*

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Torque

$$T_f = \frac{I_{fm} B_o A}{4} * \left[\cos \phi_f + \cos[2((\omega_1 - \omega)t - \theta_o) - \phi_f] \right. \\ \left. - \cos(2\omega_1 t - \phi_f) - \cos[2(\omega t + \theta_o) + \phi_f] \right]$$

$$T_{favg} = \frac{I_{fm} B_o A}{4} \cos \phi_f$$

Similarly

$$T_{bavg} = -\frac{I_{bm} B_o A}{4} \cos \phi_b$$



$$T_{net} = \frac{B_o A}{4} [I_{fm} \cos \phi_f - I_{bm} \cos \phi_b]$$

Motors: AC Motor

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$$T_{net} = \frac{B_o A}{4} [I_{fm} \cos \phi_f - I_{bm} \cos \phi_b]$$

For $\omega = 0$



$$I_{fm} = I_{bm}$$

$$\phi_f = \phi_b$$



$$T_{net} = \text{zero}$$

This motor **cannot** start from rest by its own developed torque

For any speed ω



$$I_{fm} \neq I_{bm}$$

$$\phi_f \neq \phi_b$$



$$T_{net} \neq \text{zero}$$

Motors: *AC Motor*

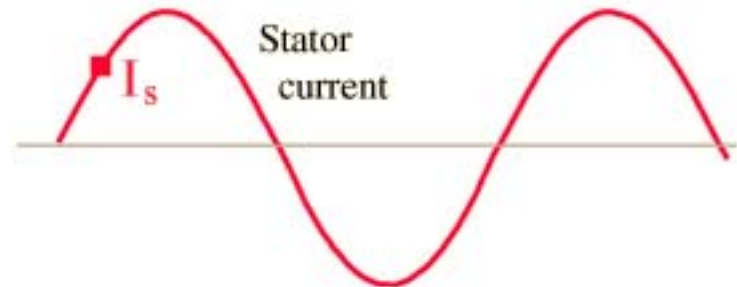
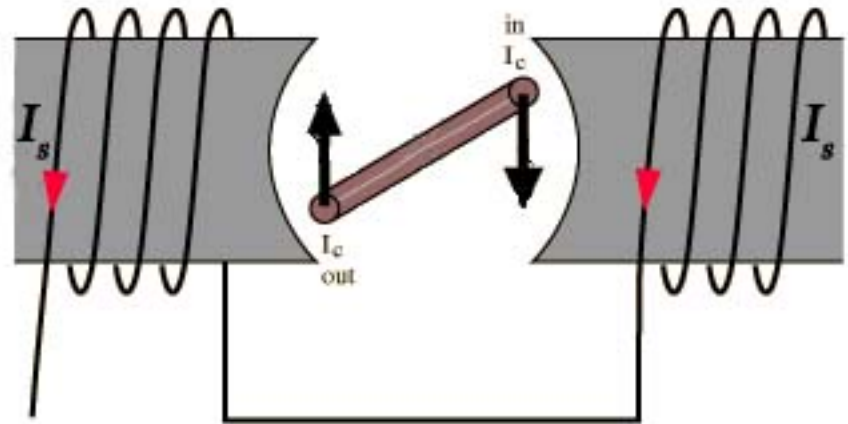
26

The motor needs an external method to start-up

It is called Induction Motor

Single Phase

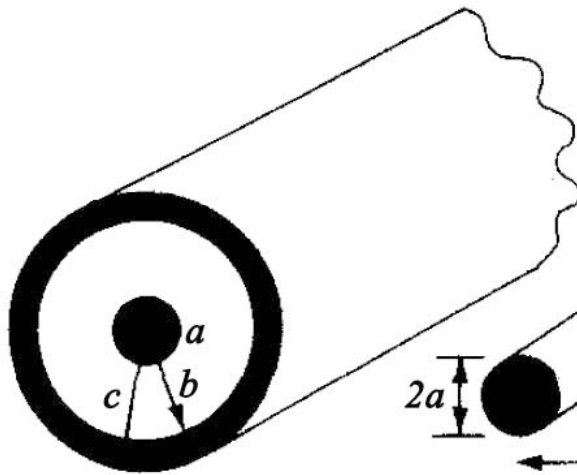
Induction Motor



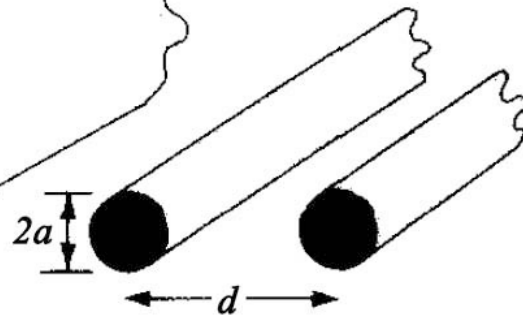
Transmission Line Parameters

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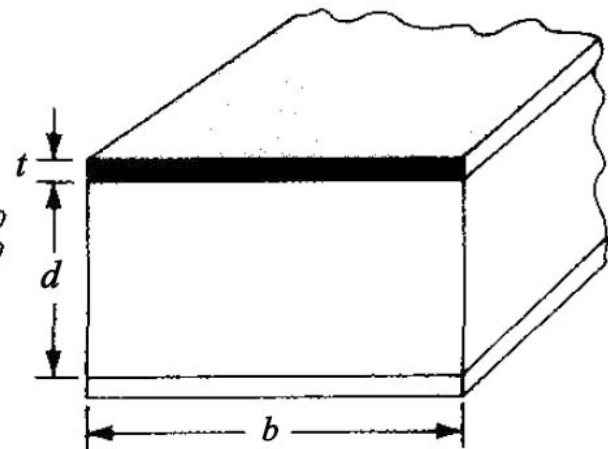
Transmission lines are used to transmit electric energy (power distribution at low frequency) and signals (communication at high frequency) from one point to another, specially from a source to a load.



Coaxial Line



Two Wire Line

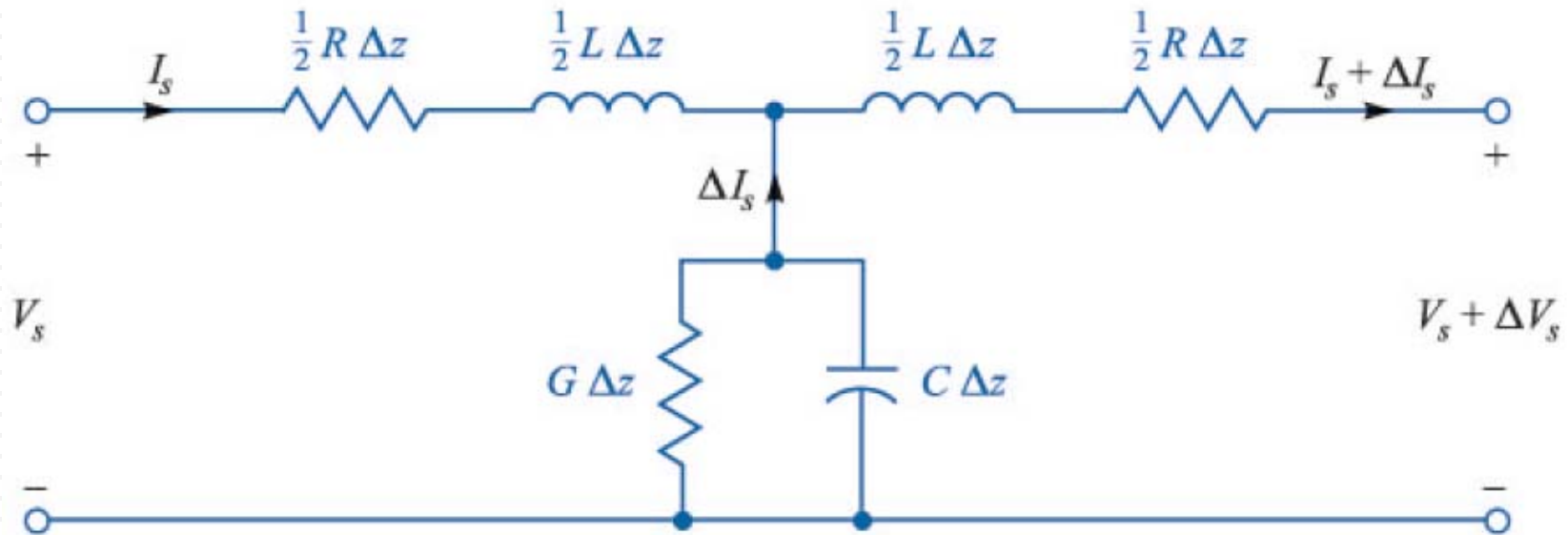


Planar Line

Transmission Line Parameters

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Transmission line circuit model



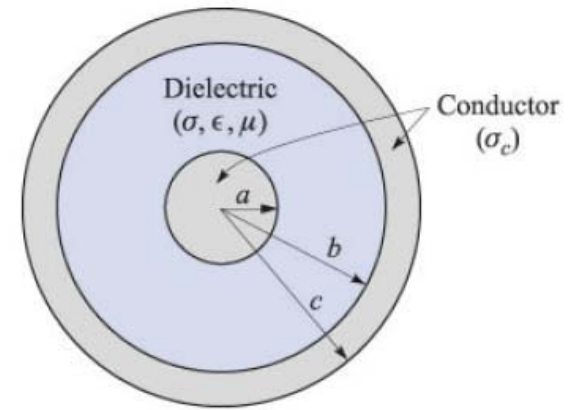
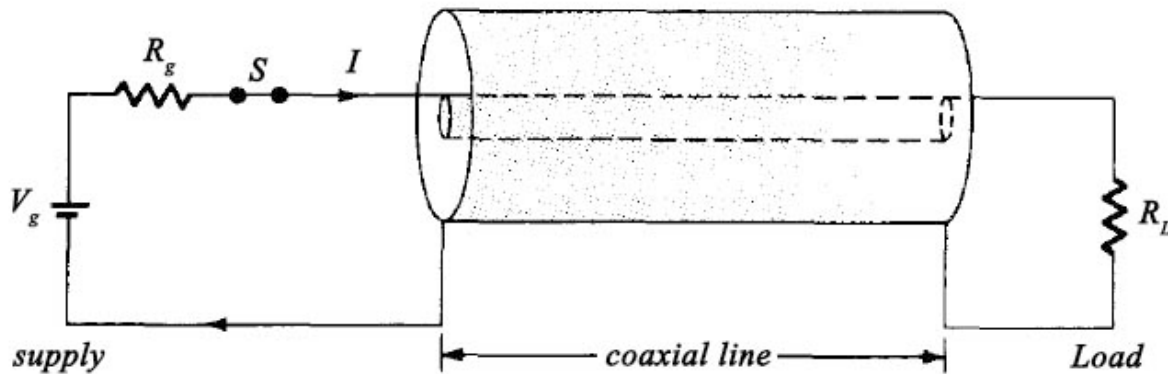
R , L , C & G are functions of the transmission line configuration and materials

Transmission Line Parameters

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1. Coaxial Line

At Low frequencies:



Resistance

$$R_{in} = \frac{1}{\sigma_c \pi a^2} \quad \boxed{\Omega / m}$$

$$R_{out} = \frac{1}{\sigma_c \pi (c^2 - b^2)} \quad \boxed{\Omega / m}$$

Transmission Line Parameters

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1. Coaxial Line

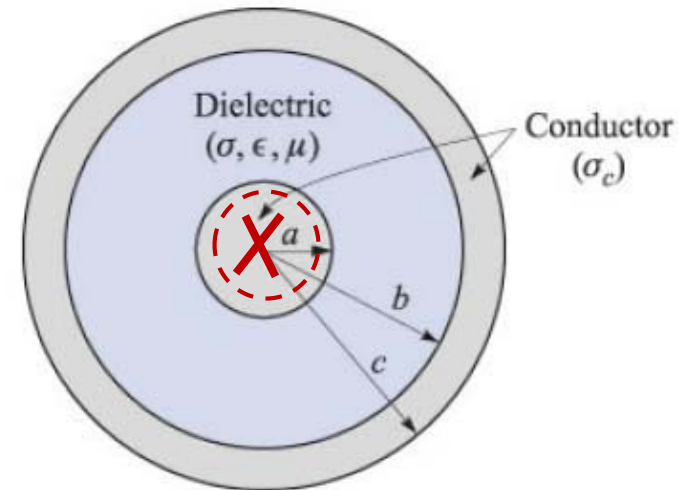
Internal Inductance

$$\underline{H} = \frac{Ir}{2\pi a^2} \underline{u}_\phi$$

$$w_e = \int \frac{1}{2} \mu H^2 dv = \frac{1}{2} LI^2$$

$$w_e = \int_{z=0}^1 \int_{r=0}^a \int_{\phi=0}^{2\pi} \frac{\mu r^2 I^2}{8\pi^2 a^4} r dr d\phi dz = \frac{\mu I^2}{16\pi}$$

$$L_{in} = \frac{\mu}{8\pi} \quad H / m$$



Transmission Line Parameters

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1. Coaxial Line

Inductance

$$\underline{H} = \frac{I}{2\pi r} \underline{u}_\phi$$

$$\underline{B} = \frac{\mu I}{2\pi r} \underline{u}_\phi$$

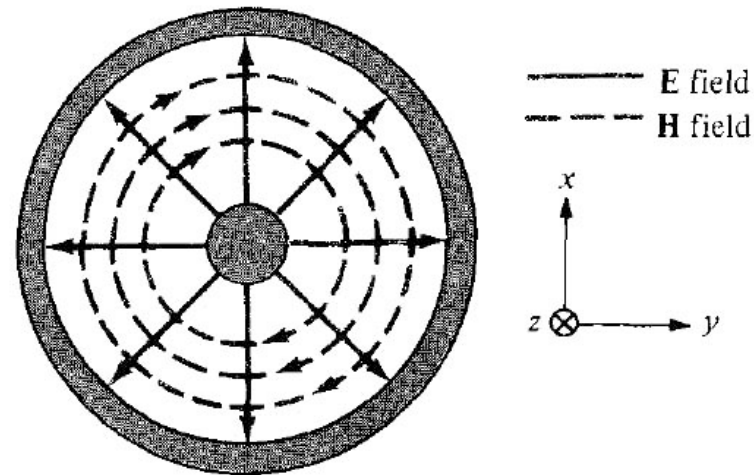
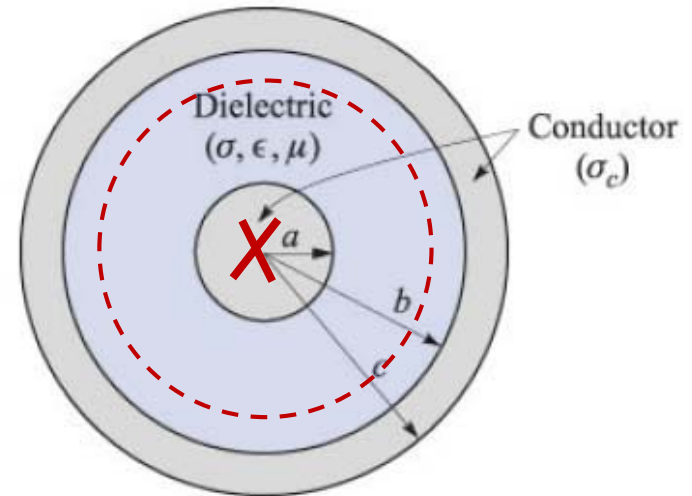
$$\lambda = N \int \underline{B} \cdot d\underline{s}$$

$$\lambda = \int_{z=0}^1 \int_{r=a}^b \frac{\mu I}{2\pi r} dr dz = \frac{\mu I}{2\pi} \ln \frac{b}{a}$$

$$L = \frac{\lambda}{I}$$

$$L = \frac{\mu}{2\pi} \ln \frac{b}{a}$$

H / m



Transmission Line Parameters

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1. Coaxial Line

Capacitance

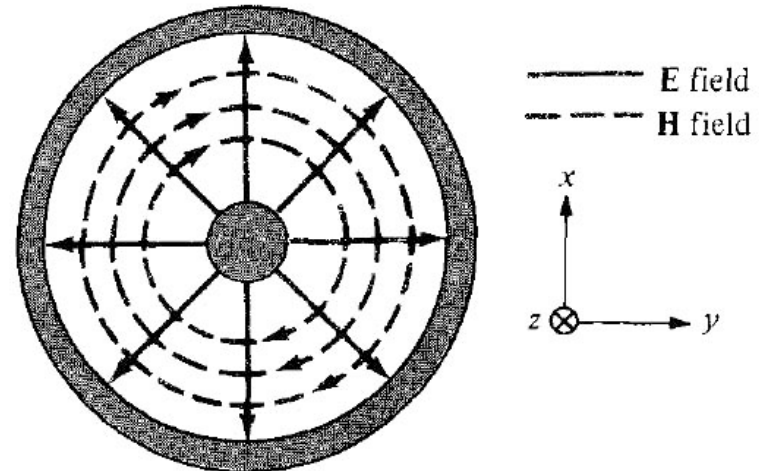
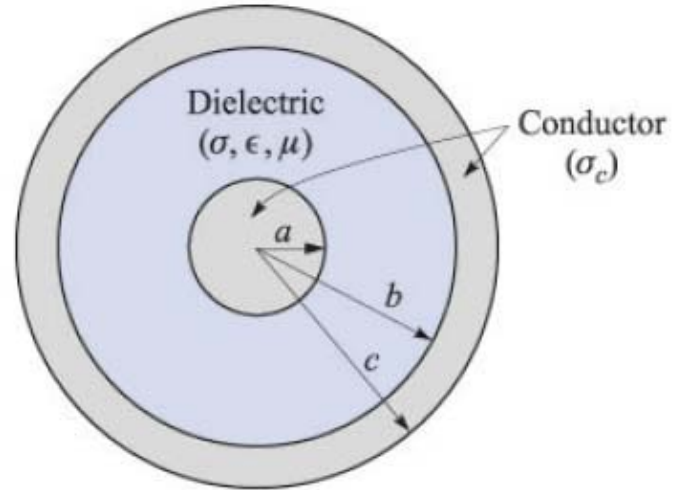
$$\underline{E} = \frac{Q}{2\pi\epsilon rL} \underline{u}_r$$

$$V_{ab} = \int_{r=a}^b \frac{Q}{2\pi\epsilon rL} dr = \frac{Q}{2\pi\epsilon L} \ln \frac{b}{a}$$

$$C = \frac{Q}{V}$$

$$C = \frac{2\pi\epsilon}{\ln b/a} \quad F / m$$

$$LC = \mu\epsilon$$



Transmission Line Parameters

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1. Coaxial Line

Conductance

$$\underline{E} = \frac{Q}{2\pi\epsilon rL} \underline{u}_r$$

$$R = \frac{\int \underline{E} \cdot d\underline{l}}{\sigma \int \underline{E} \cdot d\underline{S}} = \frac{V_{ab}}{I_L} = \frac{1}{G}$$

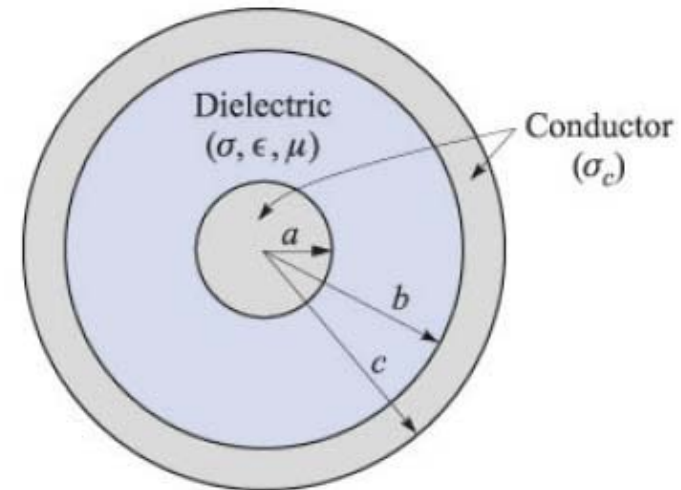
$$V_{ab} = \frac{Q}{2\pi\epsilon L} \ln \frac{b}{a}$$

$$I_L = \sigma \int_{\phi=0}^{2\pi} \int_{z=0}^L \frac{Q}{2\pi\epsilon rL} r d\phi dz = \frac{\sigma Q}{\epsilon}$$

$$G = \frac{2\pi\sigma}{\ln b/a}$$

$$\boxed{\mathcal{U} / m}$$

$$\frac{C}{G} = \frac{\epsilon}{\sigma}$$



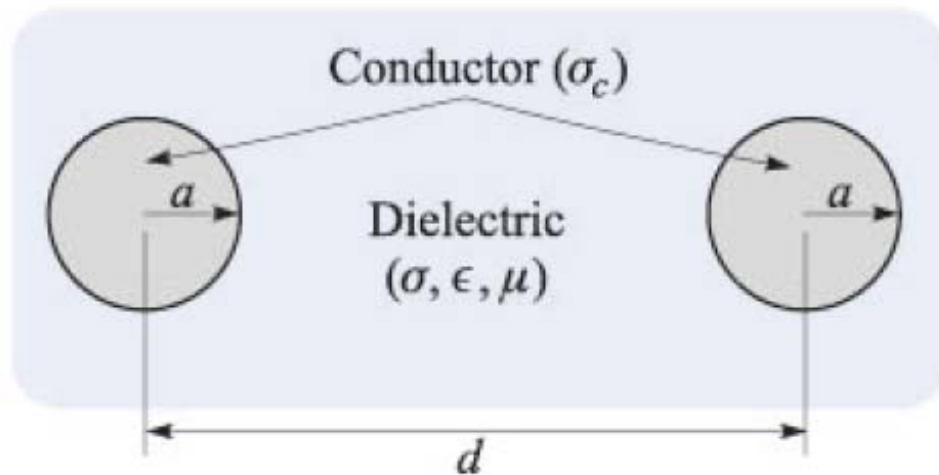
Transmission Line Parameters

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2. Two Wire Line

At Low Frequencies:

Resistance



$$R = \frac{2}{\sigma_c \pi a^2} \quad \Omega / m$$

Transmission Line Parameters

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2. Two Wire Line

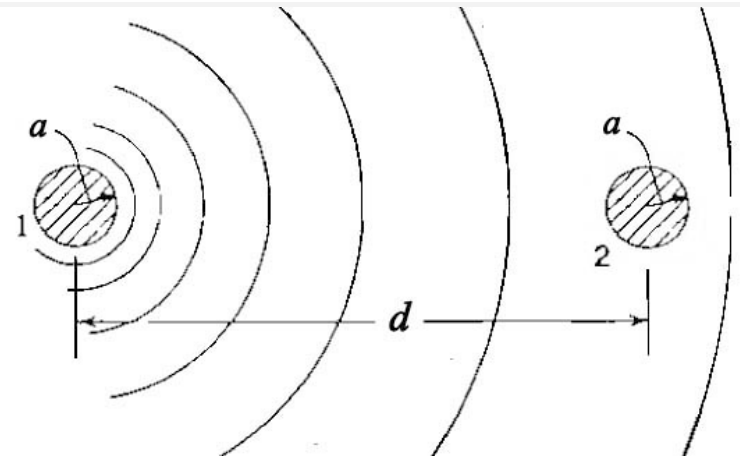
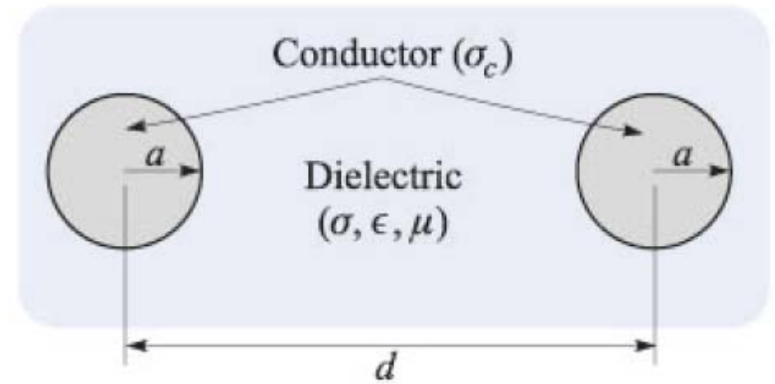
Inductance

$$\underline{H} = \frac{I}{2\pi r} \underline{u}_\phi$$

$$\underline{B} = \frac{\mu I}{2\pi r} \underline{u}_\phi$$

$$\lambda_{12} = \int_{z=0}^1 \int_{r=a}^d \frac{\mu I}{2\pi r} dr dz = \frac{\mu I}{2\pi} \ln \frac{d}{a}$$

$$L_{12} = \frac{\mu}{2\pi} \ln \frac{d}{a} \quad H / m$$



Transmission Line Parameters

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2. Two Wire Line

Inductance

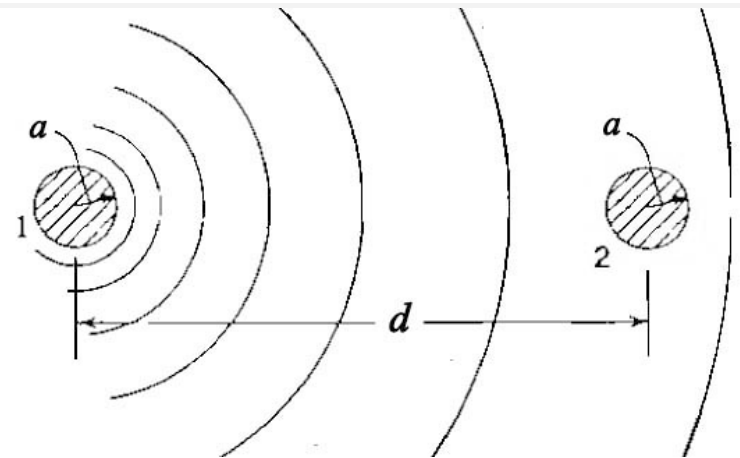
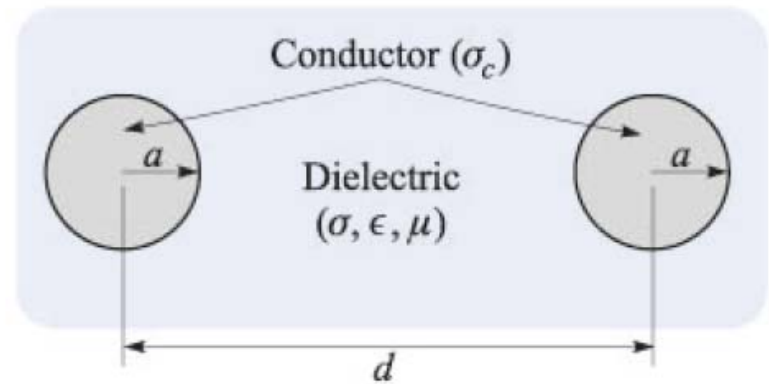
$$L_1 = L_{12} + L_{1in}$$

$$L_{in} = \frac{\mu}{8\pi}$$

$$L_1 = \left(\frac{1}{2} + 2 \ln \frac{d}{a}\right) \times 10^{-7}$$

$$L_1 = \left(\frac{1}{4} + \ln \frac{d}{a}\right) 2 \times 10^{-7}$$

$$L_1 = 2 \times 10^{-7} \ln \frac{d}{ae^{-1/4}}$$



Transmission Line Parameters

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2. Two Wire Line

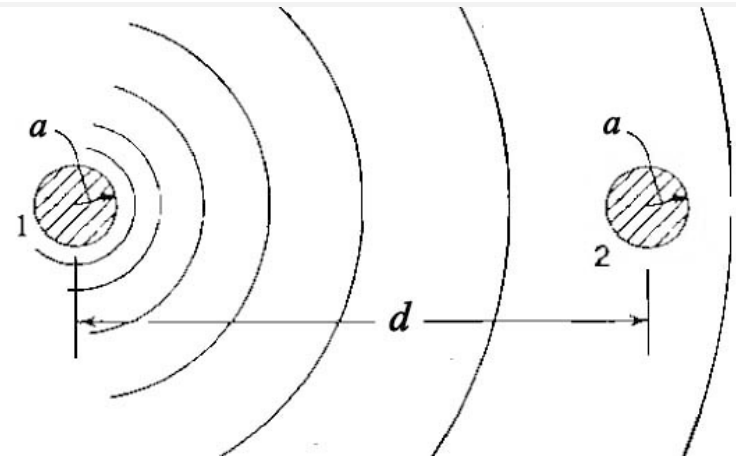
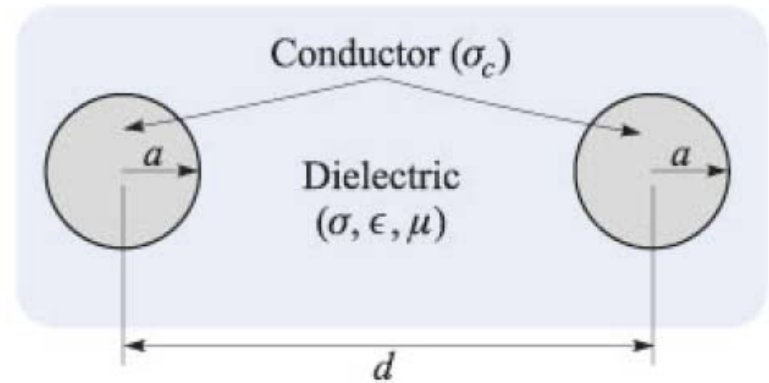
Inductance

$$L_2 = 2 \times 10^{-7} \ln \frac{d}{ae^{-1/4}}$$

$$L_{\text{circuit}} = L_1 + L_2 = 4 \times 10^{-7} \ln \frac{d}{ae^{-1/4}}$$

$$L_{\text{circuit}} = 4 \times 10^{-7} \ln \frac{d}{a'} \quad H / m$$

$$a' = ae^{-0.25}$$



Transmission Line Parameters

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2. Two Wire Line

Capacitance

$$L_{12} = \frac{\mu}{2\pi} \ln \frac{d}{a}$$

$$LC = \mu\epsilon$$

$$C_{12} = \frac{2\pi\epsilon}{\ln d/a}$$

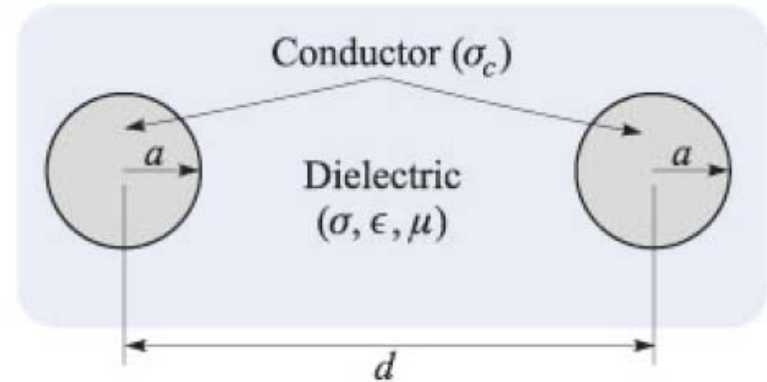
$$F / m$$

Conductance

$$\frac{C}{G} = \frac{\epsilon}{\sigma}$$

$$G_{12} = \frac{2\pi\sigma}{\ln d/a}$$

$$\mathcal{U} / m$$

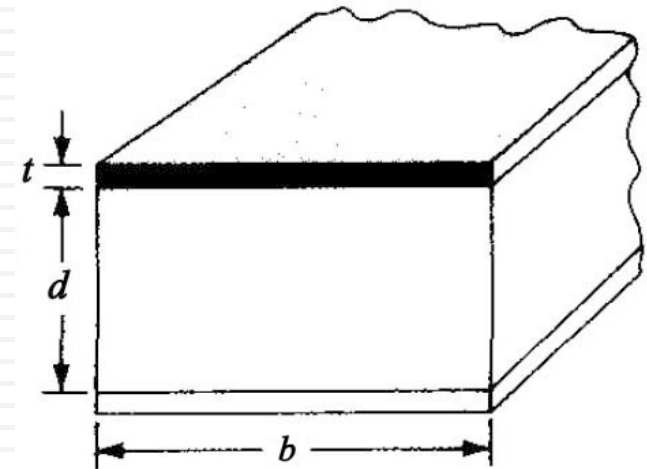
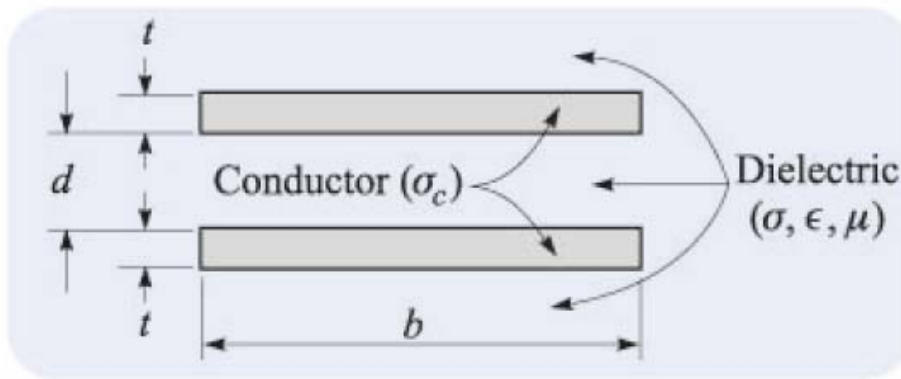


Transmission Line Parameters

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3. Planar Line

At High Frequency:



$$R = \frac{2}{\sigma \delta b} \quad \Omega / m \quad C = \frac{\epsilon b}{d} \quad F / m \quad L = \frac{\mu d}{b} \quad H / m \quad G = \frac{\sigma b}{d} \quad \mathcal{U} / m$$

$\delta = \text{skin depth}$

Transmission Line Parameters

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4. Power Lines (single-phase and three-phase)

